# **STPM32, STPM33, STPM34**

## ASSP for metering applications with up to four independent 24-bit 2<sup>nd</sup> order sigma-delta ADCs, 4 MHz OSF and 2 embedded PGLNA



life.augmented

## **Features**

- Active power accuracy:
	- <0.1% error over 5000: 1 dynamic range
	- <0.5% error over 10000: 1 dynamic range
- Exceeds 50-60 Hz EN 50470-x, IEC 62053-2x, ANSI12.2x standard requirements for AC watt meters
- Reactive power accuracy:
	- <0.1% error over 2000:1 dynamic range
- Dual mode apparent energy calculation
- Instantaneous and averaged power
- RMS and instantaneous voltage and current
- Under and overvoltage detection (sag and swell) and monitoring
- Overcurrent detection and monitoring
- UART and SPI serial interface with programmable CRC polynomial verification
- Programmable LED and interrupt outputs
- Four independent 24-bit 2<sup>nd</sup> order sigma-delta ADCs
- Two programmable gain chopper stabilized low-noise and low-offset amplifiers
- Bandwidth 3.6 kHz @ -3 dB
- $V_{cc}$  supply range 3.3 V $±10\%$
- Supply current  $I_{cc}$  4 mA (STPM32)
- Input clock frequency 16 MHz, Xtal or external source

**Datasheet** - **production data**

- Twin precision voltage reference: 1.23 V with independent programmable TC, 10 ppm/°C typ.
- Internal low drop regulator @ 3 V (typ.)
- QFN packages
- Operating temperature -40 °C~+85 °C

## **Description**

The STPM3x is an ASSP family designed for high accuracy measurement of power and energies in power line systems using the Rogowski coil, current transformer or shunt current sensors. The STPM3x provides instantaneous voltage and current waveforms and calculates RMS values of voltage and currents, active, reactive and apparent power and energies. The STPM3x is a mixed signal IC family consisting of an analog and a digital section. The analog section consists of up to two programmable gain low-noise low-offset amplifiers and up to four 2<sup>nd</sup> order 24-bit sigmadelta ADCs, two bandgap voltage references with independent temperature compensation, a low drop voltage regulator and DC buffers. The digital section consists of digital filtering stage, a hardwired DSP, DFE to the input and a serial communication interface (UART or SPI). The STPM3x is fully configurable and allows a fast digital system calibration in a single point over the entire current dynamic range.



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STPM34	STPM33	STPM32	<b>Name</b>	<b>Description and</b> multiplexed function	Voltage range	<b>Functional</b> section
23	23	17	<b>VCC</b>	Voltage supply	From 3.0 V to 3.6V	Power
24	15, 16, 24, 25		N.C.	Not connected		
25, 26	26	18	<b>GNDD</b>	Digital ground		Power
27	27	19	<b>VDDD</b>	Output of voltage regulator 1.2V	1.2V	Power
28	28	20	<b>SYN</b>	Synchronization pin	From 0 to V <sub>CC</sub>	<b>SPI</b>
29	29	21	<b>SCS</b>	Chip-select SPI/UART select	From 0 to V <sub>CC</sub>	SPI/UART
30	30	22	<b>SCL</b>	SPI clock	From 0 to $V_{CC}$	<b>SPI</b>
31	31	23	MOSI/RXD	SPI master OUT slave IN <b>UART RX</b>	From 0 to $V_{CC}$	SPI/UART
32	32	24	MISO/TXD	SPI master IN slave OUT UART TX	From 0 to $V_{CC}$	SPI/UART

**Table 2. STPM34, STPM33, STPM32 pin description (continued)**



## <span id="page-14-0"></span>**3 Absolute maximum ratings**

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#### **Table 3. Absolute maximum ratings**

*Note: Absolute maximum ratings are those values beyond which damage to the device may occur. Functional operation under these conditions is not implied. All values are referred to GND.*

#### **Table 4. Thermal data**

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*Note: This value is referred to single-layer PCB, JEDEC standard test board.*



## <span id="page-15-0"></span>**4 Electrical characteristics**

 $V_{CC}$  = 3.3 V,  $C_1$  = 1 µF between  $V_{DDA}$  and GND\_REG,  $C_1$  = 4.7 µF between  $V_{DDD}$  and GNDD,  $C_1$  = 22  $\mu$ F between V<sub>CC</sub> and GND,  $C_1$  = 100 nF between VREF1, 2 and GNDREF,  $\mathsf{F}_{\mathsf{CLK}}$ = 16 MHz, T<sub>AMB</sub> = 25 °C, EN = V<sub>CC</sub>, SPI/UART not used, unless otherwise specified.

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<b>Symbol</b>	<b>Test conditions</b> <b>Parameter</b>		rable 5. Electrical characteristics (continued) Min.	Typ.	Max.	<b>Unit</b>	
$Z_{\text{Vin}}$	Voltage channel input impedance <sup>(1)</sup>			8		MΩ	
$Z_{lin}$	Current channel input differential impedance <sup>(1)</sup>	Gain 2X Gain 4X Gain 8X Gain 16X		90 170 300 510		$k\Omega$	
$G_{ERR}$	Channel gain error	Input V <sub>MAX</sub> /2		±5		%	
	Crosstalk <sup>(1)</sup>	Voltage to current channels		$-120$		dB	
		Current to voltage channels		$-120$			
		Digital I/O (CLKOUT/ZCR, XTAL1, CLKIN/XTAL2, LED1, LED2, INT1, INT2)					
$V_{\text{IH}}$	Input high-voltage		0.75 $V_{CC}$		3.3	V	
$V_{IL}$	Input low-voltage	$V_{\rm CC} = 3.2 V$	$-0.3$		0.6	V	
$V_{OH}$	Output high-voltage	$I_{\text{O}}$ = -1 mA, C <sub>L</sub> = 50 pF, V <sub>CC</sub> = 3.2 V	$V_{CC}$ -0.4			V	
$V_{OL}$	Output low-voltage	$I_{\text{O}}$ = +1 mA, C <sub>1</sub> = 50 pF, V <sub>CC</sub> = 3.2 V			0.4	V	
	<b>Energy measurement accuracy</b>						
<b>AP</b>	Active power	Over dynamic range 5000:1, PGA = 2 to 16		0.1			
		Over dynamic range $10000:1$ , PGA = 2 to 16		0.5		%	
<b>RP</b>	Reactive power	Over dynamic range 2000:1, PGA = 2 to 16		0.1			
<b>RMS</b>	Voltage RMS	Over dynamic range 1:200		0.5		%	
	<b>Current RMS</b>	Over dynamic range 1:500		0.5			
$f_{BW}$	$-3dB$ , HPF = 1 Effective bandwidth		4		3600	Hz	
	Sigma-delta ADC performance						
<b>OSF</b>	Oversampling 4 frequency				MHz		
DR	Decimation ratio			1/512			
$F_{s}$	Sampling frequency			7.8125		kHz	
<b>FBW</b>	Flat band	$\overline{2}$ <0.05 dB allowed ripple				kHz	
BW	Effective bandwidth	$-3$ dB, HPF $=0$	$\mathbf 0$		3600	Hz	
	DC measurement accuracy						
<b>PSRR<sub>AC</sub></b>	Power supply AC rejection <sup><math>(2)</math></sup>	Voltage input shorted Current input shorted $V_{CC}$ = 3.3 V±150 mVp @ 1 kHz		65		dB	
SPI timings <sup>(3)</sup>							

**Table 5. Electrical characteristics (continued)**







1. Guaranteed by design.

2. Guaranteed by characterization.

3. Guaranteed by application.



<span id="page-18-2"></span>

### **Figure 7. SPI timings**

## <span id="page-18-0"></span>**4.1 Pin programmability**

### **Table 6. Programmable pin functions**

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<b>Name</b>	<b>Multiplexed function</b>	<b>Functional description</b>	VO.
INT <sub>1</sub>	Interrupt	Programmable interrupt 1	Output
	SD voltage (DATV1)	Sigma-delta bitstream of primary voltage	
INT <sub>2</sub>	Interrupt	Programmable interrupt 2	Output
	SD out voltage (DATV2)	Sigma-delta bitstream of secondary voltage	
<b>SCS</b>	<b>SPI/UART</b> select	Serial port selection at power-up	Output
	Chip-select	SPI/UART chip-select	
MOSI/RXD	SPI master OUT slave IN	<b>SPI</b>	Input
	<b>UART RX</b>	<b>UART</b>	
MISO/TXD	SPI master IN slave OUT	<b>SPI</b>	Output
	<b>UART TX</b>	<b>UART</b>	

**Table 6. Programmable pin functions (continued)**

1. A: active wideband; AF: active fundamental; R: reactive; S: apparent.



## <span id="page-20-0"></span>**5 Typical application example**

*[Figure 8](#page-21-0)* below shows the reference schematic of an application with the following properties:

- Constant pulses  $C_P = 43000$  imp/kWh
- $\bullet$   $I_{NOM} = 5 A$
- $I_{MAX} = 90 A$

Typical values for current sensor sensitivity are indicated in *[Table 7](#page-22-0)*.

For more information about the application dimensioning and calibration please refer to *[Section 9](#page-74-0)*.



#### **Typical application example STPM32, STPM33, STPM34**

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#### **Figure 8. STPM34 application schematic**



<span id="page-22-0"></span>

<b>Function</b>	Component	<b>Description</b>	Value	<b>Tolerance</b>		Unit
Line voltage	Resistor	R to R ratio $V_{RMS}$ =230 V	1:1650	士士		V/V
interface	divider	R to R ratio $V_{RMS}$ =110 V	1:830	1%	50 ppm/ $\mathrm{^{\circ}C}$	
	Rogowski coil		0.15	±± 5%		mV/A
Line current interface	<b>CT</b>	Current to voltage ratio $K_S$	2.4	士士 5%	50 ppm/ $\mathrm{^{\circ}C}$	
	Shunt		0.3	±± 5%		

**Table 7. Suggested external components in metering applications**

*Note: Above listed components refer to typical metering applications. The STPM3x operation is not limited to the choice of these external components.*



## <span id="page-23-0"></span>**6 Terminology**

## <span id="page-23-1"></span>**6.1 Conventions**

The lowest analog and digital power supply voltage is named GND and represents the system ground. All voltage specifications for digital input/output pins are referred to GND. The highest power supply voltage is named  $V_{CC}$ . The highest core power supply is internally generated and is named  $V_{DDA}$ . Positive currents flow to a pin. Sinking current means that the current is flowing to the pin and it is positive. Sourcing current means that the current is flowing out of the pin and it is negative. A positive logic convention is used in all equations.

<span id="page-23-5"></span>



## <span id="page-23-2"></span>**6.2 Measurement error**

The power measurement error is defined by the following equation:

#### **Equation 1**

$$
e\% = \frac{measured power - true power}{true power}
$$

All measurements come from the comparison with a higher class power (0.02% error) meter reference. Output bitstream of modulator is indicated as *bsV* and *bsC* for voltage and current channel respectively.

## <span id="page-23-3"></span>**6.3 ADC offset error**

This is the error due to DC component associated with the analog inputs of the A/D converters. Due to the internal automatic DC offset cancellation, the STPM3x measurement is not affected by DC components in voltage and current channel. DC offset cancellation is implemented in DSP thanks to a dedicated HPF.

## <span id="page-23-4"></span>**6.4 Gain error**

The gain error is due to the signal channel gain amplifiers. This is the difference between the measured ADC code and the ideal output code. The difference is expressed as percentage of the ideal code.



<span id="page-24-4"></span>45 50 55 60 65 Frequency [Hz]

## <span id="page-24-2"></span><span id="page-24-0"></span>**7 Typical performance characteristics**

<span id="page-24-1"></span>



<span id="page-24-3"></span>GIPG1403141123LM

GIPG1403141129LM

<span id="page-25-0"></span>

<span id="page-25-1"></span>**Figure 14. Reactive energy error vs. current gain=16x integrator off**



<span id="page-25-2"></span>**Figure 15. Reactive energy error vs. frequency Figure 16. Reactive energy error vs. frequency gain=2x integrator off**

<span id="page-25-3"></span>**gain=16x integrator off**





#### <span id="page-26-0"></span>**Figure 17. Active energy error vs. current gain=16x integrator on**

#### <span id="page-26-1"></span>**Figure 18. Reactive energy error vs. current gain=16x integrator on**





## <span id="page-27-0"></span>**8 Theory of operation**

### <span id="page-27-1"></span>**8.1 General operation description**

The STPM3x product family measures up to two line voltages and two line currents to perform active, reactive and apparent power and energy, RMS and instantaneous values, and line frequency information measurement of a single, split or poly-phase metering system.

The STPM3x generates up to two independent train pulse output signals proportional to the active, reactive, apparent or cumulative power. It also generates up to two programmable interrupt output signals.

The internal register map and the configuration registers can be accessed by SPI or UART interface.

The STPM3x converts analog signals, through four independent channels in parallel via sigma-delta analog-to-digital converters, into a binary stream of sigma-delta signals with the appropriate not overlapped control signal generator.

This technique fits to measure electrical line parameters (voltage and current) via analog signals from voltage sensors and current sensors (inductive Rogowski coil, current transformer or shunt resistors). Current channel inputs are connected, through external antialiasing RC filter, to a Rogowski coil or current transformer (CT) or shunt current sensor which converts line current into the appropriate voltage signal. Each current channel includes a low-noise voltage preamplifier with a programmable gain. Voltage channels are connected to a line voltage modulator (ADC). All channels have quiescent zero signal point on GND, so the STPM3x samples differential signals on both channels with their zero point around GND.

The converted sigma-delta signals feed an internal decimation filter stage that decimates 4 MHz bitstreams of a factor 512 allowing a 3.6 kHz bandwidth at -3 dB. The 24-bit voltage and current data feed an internal configurable filtering block and the hardwired DSP that performs the final computation of metrology quantities.

The STPM3x also includes two programmable temperature compensated bandgap reference voltage generators and low drop supply voltage regulator. All reference voltages are designed to eliminate the channel crosstalk.

The mode of operation and configuration of the device can be selected by dedicated configuration registers.



### <span id="page-28-0"></span>**8.2 Functional description of the analog part**

The analog part of the STPM3x consists of the following sections:

- Power management section:
	- Reference voltage generators with programmable independent temperature compensation
	- +3 V low drop supply voltage regulator
	- +1.2 V low drop supply voltage regulator
- Analog front end section:
	- Preamplifiers in the two current channels
	- 2<sup>nd</sup> order sigma-delta modulators
- Clock generator
- Power-on-reset (POR)

### <span id="page-28-1"></span>**8.2.1 Power management section**

Supply pins for the analog part are: VCC, VDDA, VDDD and GND.

GND pins represent the reference point.

VCC pin is the power supply input namely +3.3 V to GND\_REG, it has to be connected to GND\_REG via a 100 µF capacitor.

VDDA and VDDD are analog output pins of internal +3.0 V and +1.2 V low drop voltage regulators.

At least 1 µF capacitor should be connected between VDDA and GNDA. At least 1 µF capacitor should be connected between VDDD and GNDD. The input of the mentioned regulators is VCC.

There are two voltage references embedded in the STPM33 and STPM34, while the STPM32 embeds a single reference.

As described in *[Figure 19](#page-29-1)*, two EN\_REF1 and EN\_REF2 bits enable the voltage references; if a unique voltage reference is used, one of these two bits must be disabled and VREF1 and VREF2 pins must be shorted; if an external reference is used both bits must be disabled and the external reference must be connected to VREF1, VREF2 pins. VREF1 and VREF2 outputs should be connected to GNDREF via a 100 nF capacitor independently.



<span id="page-29-1"></span>

**Figure 19. Power management internal connection scheme and polarization**

Temperature compensated reference voltage generators produce VREF1 = VREF2 = 1.18 V at default settings. The primary voltage reference is always on and supplies the voltage and the primary current channel, the secondary voltage reference is by default in on-state and supplies the secondary channel.

These reference temperature compensation curves can be selected through three configuration bits: TCx[2:0] (**DSP\_CR1** and **DSP\_CR2**).

<span id="page-29-0"></span>

TCx0	TCx1	TCx2	$V_{REF}(V)$	$TC_V_{REF}$ (ppm/°C)
0	O	0	1.16	$-50$
0	$\Omega$		1.17	$-25$
0		0	1.18	0 (default)
$\mathbf{0}$			1.19	25
	$\Omega$	0	1.2	50
			1.21	75
		0	1.22	100
			1.225	125

**Table 9. Temperature compensation parameter typical values**



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**Figure 20. Temperature compensation typical curves**

### <span id="page-30-0"></span>**8.2.2 Analog front end**

Analog channel inputs of voltages VIP1, VIN1, VIP2, VIN2 and currents IIP1, IIN1; IIP2, IIN2 are fully differential.

Voltage channels have a preamplification gain of 2, which defines the maximum differential voltage on voltage channel inputs to  $\pm$  300 mV.

Current channels have a programmable gain selectable among 2, 4, 8 and 16, which defines the maximum differential voltage on current channel to ±300 mV, 150 mV, 75 mV or ±37.5 mV respectively. The selection is given by GAINx[1:0] (**DFE\_CR1**, **DFE\_CR2**) bits as described in the following table:

<span id="page-30-1"></span>

<b>GAINx0</b>	GAINx1	Gain	<b>Differential input</b>
		X2	$±300$ mV
		X4	$±150$ mV
		X8	$±75$ mV
		X16	$±37.5$ mV

**Table 10. Current channel input preamplifier gain selection**

The oversampling frequency of the modulators is 4 MHz, the output bitstreams of the 2<sup>nd</sup> order sigma-delta modulators relative to the voltage and to the two current channels are available on INT and LED output pins through the proper configuration (see configuration bit map).



<span id="page-31-0"></span>

**Figure 21. Analog front end internal scheme**

PLNA uses the chopping technique to cancel the intrinsic offset of the amplifier.

A dedicated block generates chopper frequencies for voltage and current channels.

The amplified signals are fed to the  $2<sup>nd</sup>$  order sigma-delta modulator.

The analog-to-digital conversion in the STPM3x is carried out using four  $2^{nd}$  order sigmadelta converters. A pseudo-random block generates pseudo-random signals for voltage and current channels. These random signals implement the dithering technique in order to decorrelate the output of the modulators and avoid accumulation points on the frequency spectrum. The device performs A/D conversions of analog signals on four independent channels in parallel.

<span id="page-31-1"></span>

**Figure 22. Block diagram of the modulator**



The sigma-delta modulators convert the input signals into a continuous serial stream of "1" and "0" at a rate determined by the sampling clock. In the STPM3x, the oversampling clock is equal to 4 MHz.

1-bit DAC in the feedback loop is driven by the serial data stream. DAC output is subtracted from the input signal and from the integrated error. If the loop gain is high enough, the average value of DAC output (and therefore the bitstream) can approach to the input signal level. When a large number of samples are averaged, a very precise value of the analog signal is obtained. This average is described in DSP section.

The converted sigma-delta bitstreams of voltage and current channels are fed to the internal hardwired DSP unit, which decimates, filters and processes those signals in order to boost the resolution and to yield all necessary signals for computations.

### <span id="page-32-0"></span>**8.2.3 Clock generator**

All the internal timing of the STPM3x is based on the input clock signal, namely 16 MHz. This signal can be provided in two different ways:

- 1. External quartz: the oscillator works with an external crystal
- 2. External clock: the XTAL1 pin can be fed by an external 16 MHz clock signal

The clock generator is powered by the analog supply and is responsible for two tasks. The former delays the turn-on of some function blocks after POR in order to help a smooth start of external power supply circuitry by keeping off all major loads. The latter provides all necessary clocks for analog and digital parts.

<span id="page-32-2"></span>

#### **Figure 23. Different oscillator circuits (a): with quartz; (b): with external source**

From the external 16 MHz clock, the entire clock tree is generated. All internal clocks have 50% duty cycle.



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<b>CLK</b> name	<b>Typical value</b> <b>Name</b>		<b>Description</b>		
Analog sampling clock	<b>SCLK</b>	4 MHz	OSF of sigma-delta modulators		
DCLK Decimated clock		7.8125 kHz	Sampling frequency of instantaneous voltage and current values		

**Table 11. Clock tree (continued)**

CLKOUT pin can be used to feed the clock with 16 MHz. When the STPM3x is used in cascade with the STPM3x or when the STPM3x is used to feed the companion MCU clock input.



<span id="page-33-1"></span>

### <span id="page-33-0"></span>**8.2.4 Power-on-reset (POR) and enable (EN)**

The STPM3x contains a power-on-reset (POR) circuit which delays the startup of the digital domain about 750 µs. If VCC supply is less than 2.5 V the STPM3x goes to the inactive state, all functions are blocked asserting a reset condition. This is useful to assure the correct device operation during the power-up and power-down.

POR sequence is illustrated in *[Figure 25](#page-34-1)*: after the start of two LDOs and internal *PowerOK* signals are asserted, the analog block first and the digital block after start the processing.



<span id="page-34-1"></span>

**Figure 25. Power-on-reset sequence**

The STPM3x also has an enable pin (EN) which works as follows:

- EN is high: when the power is on and EN pin raises, the device is enabled and starts after POR procedure as above described.
- EN is low: when the power is on and EN pin has a transition high to low, the device is disabled. It stops and the internal digital memory is cancelled so a new initialization is needed when EN goes back to high.

## <span id="page-34-0"></span>**8.3 Functional description of the digital part**

Each voltage and current channel has an independent digital signal processing chain, which is composed of:

- Digital front end (DFE)
- Phase compensation
- Decimation
- Filters
- Calibration

The outcoming signals are fed to a common hardwired DSP, which processes the metrology data.



<span id="page-35-3"></span>

**Figure 26. DSP block functional description**

### <span id="page-35-0"></span>**8.3.1 Digital front end (SDSx bits)**

This block synchronizes and checks the sigma-delta bitstreams of voltage and current signals.

Each channel sigma-delta stream has an **SDS**x status bit associated, which is cleared if the stream is correct, while it is set if the bitstream is stuck to 0 or 1 (this is the case of an input waveform saturating the dynamic input of the sigma-delta modulator).

To set SDSx bit, sigma-delta ( $\Sigma\Delta$ ) stream should be stuck to 0 or 1 for a time between:

$$
t_{\Sigma\Delta stuck} = 2/(MCLK/256) = 128 \mu s ... t_{\Sigma\Delta stuck} = 3/(MCLK/256) = 192 \mu s
$$

Outputs are stored on bit number: 0, 12, 24 of register DSP status at row 10.

If SDSx=1, the instantaneous values of voltage current are set on positive or negative maximum value, according to sigma-delta stream. In this case active powers and energies are calculated with those values of signals.

If sigma-delta stream of voltage channel is stuck, the reactive energy is zero.

### <span id="page-35-1"></span>**8.3.2 Decimation block**

The decimation block operates a serial decimation of three sigma-delta serial bitstreams coming from three modulators of voltage, primary and secondary current channels.

The decimation ratio, out of the filter cascade, is 512 so that outputs of this block are parallel 24-bit data at a rated frequency of 7.8125 kHz.

The decimation block has a magnitude response -3 dB band of 3.6 kHz and a 2.0 kHz flat band.

### <span id="page-35-2"></span>**8.3.3 Filter block**

The block includes:

- DC cancellation filter (BHPFVx, BHPFCx bits)
- Rogowski coil Integrator (ROCx bit)
- Fundamental harmonic component filter
- Harmonic content selection for reactive energy (BLPFVx, BLPFCx bits)

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**Figure 27. Filter block diagram**

## **DC cancellation filter**

This block removes the DC component of signal from voltage and current signals.

It is a selectable block which can be bypassed in case of particular needs with **BHPFVx** and BHPFCx bits in **DSP\_CR1** and **DSP\_CR2**.

The filter has a passband at -3 dB of 8 Hz

 $BHPFVx = 0$ : voltage HPF is included for x channel

 $BHPFVx = 1$ : voltage HPF is bypassed for x channel

 $BHPFCx = 0$ : current HPF is included for x channel

 $BHPFCX = 1$ : current HPF is bypassed for x channel

## **Rogowski coil Integrator**

ROCx bit in **DSP\_CR1** and **DSP\_CR2** selects the type of current sensors (CT, shunt or Rogowski coil):

ROCx = 0: channel x current sensor is CT or shunt

ROCx = 1: channel x current sensor is Rogowski coil

In case of  $ROCx = 1$ , integrator filter is included to integrate current signal coming from Rogowski coil current sensor. Rogowski coil integrator is selectable independently for each current channel.

## **Fundamental component filter**

This low-pass filter on the voltage and current signals is used to calculate: zero-crossing, period, phase-angles and fundamental active and reactive energy. Filtered voltage and current components are available on **DSP\_REG6**, **DSP\_REG7**, **DSP\_REG8**, **DSP\_REG9** named *VxFund* and *CxFund*.



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## **Reactive filter**

Reactive filter introduces a delay in current and voltage streams respectively; these signals are used to calculate reactive power and energy.

Input streams for reactive filter are selectable for each voltage and current channel signals between signals without harmonic (*VxFund* and *CxFund*) or full bandwidth signals *(VxData*, *CxData*) through BLPFVx and BLPFCx configuration bits in **DSP\_CR1** and **DSP\_CR2**.

 $BLPFVx = 0$ : voltage LPF is included for x channel

 $BLPFVx = 1$ : voltage LPF is bypassed for x channel

 $BLPFCX = 0$ : current LPF is included for x channel

BLPFCx = 1: current LPF is bypassed for x channel

If LPF is bypassed, full bandwidth data are used to calculate the reactive energy; if LPF is included, fundamental data are used.

# **8.4 Functional description of hardwired DSP**

From the decimation and filtering block, signals are fed to hardwired DSP to compute the following quantities for primary and secondary channels:

- Active power and energy wideband 0 Hz(4 Hz)-3.6 kHz
- Active power and energy fundamental 45-65 Hz
- Reactive power and energy selectable on fundamental harmonic or on full bandwidth
- Apparent power and energy from RMS data
- Apparent power vectorial calculation
- Signal measurement: RMS, period, zero-crossing, phase-delay, sag and swell, tamper

Each power signal is accumulated in the correspondent energy register every 7.8125 kHz.

Energy registers are up-down counters. The accumulation is signed so that the negative energy is subtracted from the positive energy. When the measured power is positive, the energy register increases its content from 0x00000000 up to the maximum value, 0xFFFFFFFF, then it rolls from 0xFFFFFFFF back to 0x00000000.

Vice versa, when the power is negative, the register decreases its content; from 0x00000000 rolls to 0xFFFFFFFF and continues decreasing till 0x00000000.

To monitor each energy register overflow and power sign change, status bits are available on **DSP\_SR1** and **DSP\_SR2**.

When a selectable threshold is reached, a pulse is generated on LED pin.

This threshold is selectable through a set of configuration bit (LPWx[3:0] in **DSP\_CR1** and **DSP\_CR2**) as shown in *[Table 12](#page-38-0)*. For each bit configuration, LED signal goes high when the two selected bits commute to 10 and goes low when the two selected bits change to 11. Maximum LED pulse width is anyway fixed to 81.92 ms (640 periods of 7812.5 Hz clock).



<span id="page-38-0"></span>

<b>LPWx</b>	<b>Division factor</b>
0000	0,0625
0001	0,125
0010	0,25
0011	0,5
0100	1
0101	$\sqrt{2}$
0110	$\overline{4}$
0111	$\bf 8$
1000	$16\,$
1001	32
1010	64
1011	128
1100	256
1101	512
1110	1024
1111	2048

**Table 12. LPWx bits**

The signal chain for each power, energy calculations and related frequency conversion are explained in the following section.







**Figure 28. DSP block diagram**

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# **8.4.1 Active power and energy calculation**

The signal chain for the active power, energy calculations and related frequency conversion are shown in *[Figure 29](#page-40-0)*. The instantaneous power signal *p(t)* is generated by multiplying the current and voltage signals. This value can be compensated by the active power offset calibration block (OFAx[8:0] in **DSP\_CR9** and **DSP\_CR11** registers). DC component of the instantaneous power signal (average power) is then extracted by LPF (low-pass filter) to obtain the active power information.

<span id="page-40-0"></span>



The active power is calculated simultaneously and independently for primary and secondary current channels.

Results of the calculated quantities are stored in the registers as follows:

 $EP_1$  = primary current channel active energy PH1 ACTIVE Energy[31:0]

 $P_1$  = primary current channel active power PH1 Active Power[28:0]

 $p_1(t)$  = primary current channel instantaneous active power PH1 Momentary Active Power[28:0]

 $EP<sub>2</sub>$  = secondary current channel active energy PH2 Active Energy[31:0]

 $P_2$  = secondary current channel active power PH2 Active Power[28:0]

 $p_2(t)$  = secondary current channel instantaneous active power PH2 Momentary Active Power[28:0]

Active power measurements have a bandwidth of 3.6 kHz and include the effects of any harmonic within that range.

## **8.4.2 Fundamental active power and energy calculation**

The signal chain for the fundamental active power, energy calculations and related frequency conversion are shown in *[Figure 30](#page-41-0)*. The signal flow is the same as the active energy wideband, but voltage and current waveforms are filtered to remove all harmonic components but the first (45-65 Hz). Power value can be compensated by the active power offset calibration block (OFAFx[8:0] in **DSP\_CR9** and **DSP\_CR11**).



<span id="page-41-0"></span>

**Figure 30. Fundamental active power and energy calculation block diagram**

Results of the calculated quantities are stored in the registers as follows:

 $EF_1$  = primary current channel active fundamental energy PH1 Fundamental Energy[31:0]

 $F_1$  = primary current channel active fundamental Power PH1 Fundamental Power[28:0]

 $f_1(t)$  = primary current channel instantaneous active fundamental power PH1 Momentary Fundamental Power[28:0]

 $EF<sub>2</sub>$  = secondary current channel active fundamental energy PH2 Fundamental Energy[31:0]

 $F<sub>2</sub>$  = secondary current channel active fundamental power PH2 Fundamental Power[28:0]

 $f_2(t)$  = secondary current channel instantaneous active fundamental power PH2 Momentary Fundamental Power[28:0]

The fundamental active power measurements have a bandwidth of 80 Hz.

## **8.4.3 Reactive power and energy calculation**

The signal chain for the reactive power, energy calculations and related frequency conversion are shown in *[Figure 31](#page-42-0)*. The instantaneous reactive power signal is generated by multiplying the filtered signals of current and voltage. This value can be compensated by the reactive power offset calibration block (OFRx[8:0] in **DSP\_CR10** and **DSP\_CR12**). The DC component of the instantaneous power signal is extracted from LPF to obtain the reactive power information.



<span id="page-42-0"></span>

**Figure 31. Reactive power and energy calculation block diagram**



Results of the calculated quantities are stored in the registers as follows:

 $EQ<sub>1</sub>$  = primary current channel reactive energy PH1 Reactive Energy[31:0]

 $Q_1$  = primary current channel reactive power PH1 Reactive Power[28:0]

 $q_1(t)$  = primary current channel instantaneous reactive power PH1 Momentary Reactive Power[28:0]

 $EQ<sub>2</sub>$  = secondary current channel reactive energy PH2 Reactive Energy[31:0]

 $Q<sub>2</sub>$  = secondary current channel reactive power PH2 Reactive Power[28:0]

 $q_2(t)$  = secondary current channel instantaneous active power PH2 Momentary Reactive Power[28:0]

The signal bandwidth for reactive power measurement is selected by **BLPFVx** and **BLPFCx** configuration bits.

## **8.4.4 Apparent active power and energy calculation**

The signal chain for the apparent power, energy calculations and related frequency conversion are shown in *[Figure 32](#page-44-0)*. The apparent power signal S is generated in two ways:

• Vectorial methodology uses the scalar product of active and reactive power. The active power is selectable through the active power mode bit (APMx in **DSP\_CR1** and **DSP\_CR2**) between wideband or fundamental. Wideband or fundamental reactive power calculation is selected by BLPFVx and BLPFCx bits:

#### **Equation 2**

$$
S_{\text{vec}} = \sqrt{P^2 + Q^2}
$$

• RMS methodology uses the product of RMS data of voltage and current. This value can be compensated by the apparent power offset calibration block (OFSx[8:0] in **DSP\_CR10** and **DSP\_CR12**).

## **Equation 3**

$$
S_{RMS} = V_{RMS} \cdot I_{RMS}
$$

The apparent energy is calculated from vectorial or from RMS apparent power according to AEMx configuration bit in **DSP\_CR1** and **DSP\_CR2**.



<span id="page-44-0"></span>



Results of the calculated quantities are stored in the registers as:

 $ES_1$  = primary current channel apparent energy PH1 Apparent Energy[31:0]

 $S<sub>1RMS</sub>$  = primary current channel apparent RMS power PH1 Apparent RMS Power[28:0]

 $S<sub>1</sub>vec$  = primary current channel apparent vectorial power PH1 Apparent Vectorial Power[28:0]

 $ES<sub>2</sub>$  = secondary current channel apparent energy PH2 Apparent Energy[31:0]

 $S_{2RMS}$  = primary current channel apparent RMS power PH2 Apparent RMS Power[28:0]

 $S<sub>1</sub>vec$  = primary current channel apparent vectorial power PH2 Apparent Vectorial Power[28:0]

## **8.4.5 Sign of power**

Power measurements are signed calculations. Negative power indicates that energy has been injected into the grid. **DSP\_SR1**, **DSP\_SR2** status registers and **DSP\_EV1**, **DSP\_EV2** registers include sign indication bits for each calculated power.

If the sign of power is negative, the sign bit is set.

SIGN = 0: positive power

SIGN = 1: negative power

In the calculation of the sign, a delay equal to half line period is included.

If the period of signal is  $T = 20$  ms (f = 50 Hz), the applied delay is 10 ms.



**Figure 33. Power sign status bit delay**



# **8.4.6 Calculation of power and energy**

In the following section, constant parameters, coming from the device architecture, are used:

<span id="page-45-0"></span>

<b>Parameter</b>	Value		
Voltage reference	$V_{RFF} = 1.18$ [V]		
Decimation clock	DCLK=7812.5 [Hz]		
Integrator gain (for Rogowski coil only)	$k_{int} = 1$	if ROC bit = $0$ in <b>DSP CR1,2</b>	
	if $\overline{ROC}$ bit = 1 in <b>DSP_CR1,2</b> $k_{\text{int}} = 0.8155773$		
RMS block gain	$k_{RMS} = 0.6184$		

**Table 13. STPM3x internal parameters**



Basic calculations are listed in *[Table 14](#page-46-0)*:

<span id="page-46-0"></span>





<u>1991 - 1912 MINA DUSIO CUIONIQUOIIS (CONTINUOT</u>					
<b>Parameter</b>	<b>Voltage</b>	<b>Current shunt</b>	<b>Current CT</b>	<b>Current Rogowski coil</b>	
Power LSB value	$LSB_P = \frac{P_{pulse}}{2^{29}} \cdot DClk = \frac{LED\_PWM \cdot V_{ref}^2 \cdot \left(1 + \frac{R_1}{R_2}\right)}{k_{int} \cdot A_V \cdot A_I \cdot k_S \cdot cal_V \cdot cal_V \cdot 2^{28}} \left[\frac{W}{LSB}\right]$				
Energy LSB value		$LSB_E = \frac{P_{pulse}}{2^{18}} = \frac{LED\_PWM \ V_{ref}^2 \ (1 + \frac{R_1}{R_2})}{3600 \cdot DClk \cdot k_{int} \ A_1 \cdot k_S \cdot cal_V \cdot cal_V \cdot 2^{17}} \left[\frac{Wh}{LSB}\right]$			

**Table 14. STPM3x basic calculations (continued)**

1. CHVx and CHIx calibrator bits introduce in the signal processing a correction factor of ±12,5% (with an attenuation from 0,75 to 1). In order to have the maximum available up/down correction range, by default calibrator values are in the middle<br>of their range (0x800) corresponding to an attenuation factor cal<sub>V</sub> = cal<sub>I</sub> = 0,875.

2. Σ∆ bitstream should be kept lower than 0.5 (50%) to minimize modulator distortions.

3. LPWx is the LED frequency divider that can be set in **DSP\_CR1** and **DSP\_CR2** control registers for primary and secondary current channels respectively. Default value is 1.

> For each power register, a configurable offset value (default  $= 0$ ) can be added to the instantaneous power p(n) through OFA[9:0], OFAF[9:0], OFR[9:0], OFAS[9:0] bits in this way:

## **Equation 4**

$$
p^{'}(n) = p(n) + (-1)^{OFx[9]} \cdot OFx[8:0] \times 2^2
$$

## **8.4.7 RMS calculation**

RMS block calculates RMS currents and voltages on each phase every second, according to the following formulas:

**Equation 5**

$$
V_{RMS} = \sqrt{\frac{1}{T} \int_{t_0}^{t_0 + T} v(t) dt}
$$

**Equation 6**

$$
I_{RMS} = \sqrt{\frac{1}{T} \int_{t_0}^{t_0 + T} i(t) dt}
$$

with  $T = 1$  second.

RMS block architecture is shown in *[Figure 34](#page-48-0)*:



<span id="page-48-0"></span>

If the cut-off frequency of an LP filter is set much below the input signal spectrum, it can be considered as an average operator. In this case and according to the figure, the first LP filter averages its input signal which is produced by division and multiplication:

#### **Equation 7**

$$
R = \overline{\left(\frac{X^2}{R}\right)}
$$

By assumption, the feedback signal R is DC type and therefore, it can be extracted from the average operation and the above equation can be rearranged into:

#### **Equation 8**

$$
R = \overline{(X^2)}
$$

By a square-root operation on both sides of previous equation we get:

#### **Equation 9**

$$
R = \sqrt{\overline{(X^2)}}
$$

which is RMS value exact definition.

With an AC input signal:

## **Equation 10**

$$
x = x(t) = A\sin(\omega t)
$$

$$
x^{2} = A^{2} sin^{2}(\omega t) = \frac{A^{2}(1 - cos(2\omega t))}{2}
$$



The LP filter cuts the  $2<sup>nd</sup>$  harmonic component of input signal multiplying it by a dumping factor:

**Equation 11**

$$
R = A \sqrt{\left(\frac{(1 - \alpha \cos(2\omega t))}{2}\right)} \sim \frac{A}{\sqrt{2}} \left(1 - \frac{\alpha}{2} \cos(\omega t)\right)
$$

**Equation 12**

 $R \sim \frac{A}{\sqrt{2}}$ 

R result is a DC signal plus the  $2^{nd}$  harmonic ripple with the amplitude of  $\alpha/2$ . For dumping factor | α |<<1:

## **Equation 13**

 $R \sim \frac{A}{\sqrt{2}}$ 

RMS data are available in **DSP\_REG14** and **DSP\_REG15** registers.

Raw data are also available for post-processing by MCU in registers from **DSP\_REG2** to **DSP\_REG9**.

By taking into account the internal parameters in *[Table 13](#page-45-0)* and the analog front end components in *[Table 14](#page-46-0)*, LSB values of voltage and current registers are the following:







$14000$ TV: 0.1. MOA VALLOIR TVRAGU 2012 TARAOU (UVIRIRIUM)			
<b>Parameter</b>	Value		
Instantaneous voltage LSB value	$LSB_{V_{MOM}} = \frac{V_{ref}\cdot\left(1+\frac{R_1}{R_2}\right)}{\sqrt{2}\cdot k_{RMS}\cdot A_V\cdot 2^{23}}[V]$		
Instantaneous current LSB value	$LSB_{I_{MOM}} = \frac{V_{ref} \cdot k_S}{\sqrt{2} \cdot k_{RMS} \cdot A_I \cdot 2^{23}} [A]$		

**Table 15. STPM3x current voltage LSB values (continued)**

# **8.4.8 Zero-crossing signal**

Zero-crossing signals of voltage and current come from fundamental values of voltage and current and output from LPF filter. Resolution of the zero-crossing signal is 8 μs given by  $F_{CLK}$  clock = 125 kHz.



**Figure 35. Zero-crossing generation**

*ZRC* signal is delayed by an instantaneous voltage current signal: 5.1 ms (typical), as shown in *[Figure 36](#page-50-0)*:

## **Figure 36. Zero-crossing signal**

<span id="page-50-0"></span>



## **8.4.9 Phase meter**

Phase meter detects:

- The period of the voltage line
- The phase-angle delay between voltage and current





## **Period measurement**

Starting from *ZRC* signals, line period and voltage/current phase shift are calculated.

Period information for the two phases is located in **DSP\_REG1** register.

The measurement of the period is from *ZRC* signal of voltage channel. The period is calculated like an average of last eight measured periods.

The initial values of period are set on 0x9C4 (2500). LSB of period is 8  $\mu$ s given by F<sub>CLK</sub> clock = 125 kHz. Limits to consider the correct period are between 0x600 (1536) and 0x800 (3840) corresponding to a frequency range between 32.55 and 81.38 Hz.

If the voltage signal frequency is out of this range, PER\_ERR status bit is set in **DSP\_SR1/2**.

PER  $ERR = 0$ : period in the range

PER\_ERR = 1: period out of range

When PER\_ERR bit is set, PHx\_PERIOD[11:0] is not updated and keeps the previous correct value.

## **Phase-angle measurement**

From the period information, the device calculates phase-delay between voltage and current for the fundamental harmonic.

Cx\_PHA[11:0] data for primary and secondary channel are located in **DSP\_REG17** and **DSP\_REG19** respectively.

Phase-angle φ in degrees can be calculated from the register value as follows:



**Equation 14**

$$
\varphi = \frac{Cx\_PHA[11:0]}{FClk} \cdot f \cdot 360^{\circ}
$$

Resolution at 50 Hz is:

**Equation 15**

$$
\Delta_{PhaseAngle} = \frac{0x001}{125 \, kHz} \cdot 50 \, Hz \cdot 360^{\circ} = 0.144^{\circ}
$$

When PER\_ERR bit is set, Cx\_PHA[11:0] is not updated and keeps the previous correct value.

#### **Sag and swell detection**

The device can detect and monitor the undervoltage (also called voltage dip or sag) and the overvoltage or overcurrent events (swell).

A 4-bit event register stores every time that the sag or swell condition is verified. The event history is stored in **DSP\_EV1** and **DSP\_EV2** registers as SAGx\_EV[3:0], SWVx\_EV[3:0] and SWCx\_EV[3:0]. From the event register, interrupts can be generated, and the event duration is stored in time registers: from **DSP\_REG16** to **DSP\_REG19**.

To correctly detect the event, thresholds have to be set from **DSP\_CR5** to **DSP\_CR8** as explained below.

To clear event history and time registers, once the event has been detected, ClearSS bit in **DSP\_CR1**, **DSP\_CR2** has to be set. This bit is reset automatically.

To avoid a race condition on digital counters, a time threshold CLRSS\_TO[3:0] (ClearSS time-out) can be set to delay the reset of ClearSS bit. LSB of this timeout is  $8 \mu s$ .

Status bits are also available in case of sag and swell events in **DSP\_SR1** and **DSP\_SR2**, they can give the information about the sag/swell event start or end and generate an interrupt if masked in **DSP\_IRQ1** and **DSP\_IRQ2** registers.





**Figure 38. Sag and swell detection blocks**

## **Voltage sag detection**

To detect a voltage sag, the fundamental component of voltage is compared to the 10-bit threshold SAG\_THRx[9:0] in **DSP\_CR5** and **DSP\_CR7** for primary and secondary channel respectively.

An internal time counter is incremented until momentary voltage value is below the threshold. Sag event is recorded when the timer counter reaches a programmable value set by SAG\_TIME\_THR[13:0] bits in **DSP\_CR3**. This time threshold is unique for both channels.

When a sag event is detected, LSB of SAGx EV[3:0] event register and SAG Start bit are set in the interrupt status register and an interrupt is generated.

If sag event ceases, SAGx\_EV register is left shifted and zero is added as LSB, besides, SAG end bit in the interrupt status register is set as well.

The duration of the event is stored in SAGx\_TIME[14:0] in **DSP\_REG16** and **DSP\_REG18** for primary and secondary voltage channel respectively.

If the overflow of SAG\_TIME register occurs, SAGx\_EV register is left shifted and its LSB is set, as shown in figure below.

LSB of time registers is 8 μs.

To disable sag detection, all (SAG\_THRx and SAG\_TIME\_THR) registers have be set to zero.

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## **Voltage/current swell detection**

To detect a voltage or a current swell, the fundamental component of signal is compared to the 10-bit threshold SWV\_THRx[9:0] and SWC\_THRx[9:0] in **DSP\_CR5**, **DSP\_CR6**, **DSP\_CR7**, and **DSP\_CR8**.

When the signal overcomes the threshold, a swell event is detected and LSB of SWVx\_EV[3:0] or SWCx\_EV[3:0] event register is set. At the same time, SWELL\_Start bit is set in the interrupt status register and an interrupt can be generated.

If the swell event ceases, SWV\_EV or SWC\_EV register is shifted and its LSB is set to zero, also SWELL\_End bit in the interrupt status register is set.

The duration of the event is stored in SWV\_TIME[14:0] or SWC\_TIME[14:0] in registers from **DSP\_REG16** to **DSP\_REG19** for primary and secondary voltage and current channel respectively.

If the overflow of SWV\_TIME or SWC\_TIME register occurs, the related SWVx\_EV and SWC<sub>x</sub> EV register is left shifted and its LSB is set, as shown in figure below.

LSB of time registers is 8 μs.

To disable swell detection, all registers (SWV\_THRx and SWC\_THRx) have be zero.





# **Figure 40. Swell detection process**

## **Sag and swell threshold calculation**

Thresholds for sag voltage detection are calculated below, according to the following input parameters:

V<sub>L</sub>: line voltage nominal RMS value

V<sub>SAG</sub>: target RMS value of sag voltage

R1, R2: voltage divider resistors

Au = 2, voltage channel gain

 $D_{SAG} = 2^{10}$ , length of sag threshold register

## **Table 16. Voltage sag**





#### **Table 16. Voltage sag**



To calculate the filtering time for the sag event, we consider the time in which the nominal instantaneous voltage is below the sag threshold, that is:

$$
time = 2 * \arcsin\left(\frac{V_L}{V_{SAG}}\right) * \frac{180}{\pi} * \frac{1000}{360 * f_L} [ms]
$$

To correctly distinguish between normal sinusoidal voltage and sag event, the filtering time should be added to this component, for example half line period (10 ms at 50 Hz). Since LSB of SAG\_TIME\_THRx register is 8 μs ( $F_{CLK}$  = 125 kHz), the value to set is:

#### **Equation 16**

$$
TIME = \frac{time + dt}{8 \, us} \, [HEX]
$$

In the same way:

V<sub>SWELL</sub>: target RMS value of swell voltage

Au: voltage sensor gain

 $D_{SWFI}$  = 210, length of swell threshold register

Following the above calculation we obtain the hexadecimal value of voltage swell threshold:





For the current swell, an analogue procedure can be followed:

I<sub>SWELL</sub>: target RMS value of swell current

 $K_S$ : current sensor sensitivity [V/A]

Ai: current sensor gain

The swell threshold is:



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#### **Table 18. Current swell**

## **8.4.10 Tamper detection**

The device includes a tamper detection module (the STPM34 and STPM33 only).

To enable this feature, **TMP\_EN** bit and **TMP\_TOL[1:0]** tamper tolerance have to be set in **DSP\_CR3**. Tamper detection feature is disabled by default. It is possible to choose among four different tolerances according to *[Table 19](#page-57-0)*:

<span id="page-57-0"></span>



Tamper module monitors active energy registers of the two channels. Tamper condition is detected when the absolute value of the difference between the two active energy values is greater than the chosen percentage of the averaged value. This occurs when the following equation is satisfied:

## **Equation 17**

|EnergyCH1 - EnergyCH2| > TOL \* |EnergyCH1 + EnergyCH2|/2

where TOL is selected according to *[Table 19](#page-57-0)*.

Detection threshold is much higher than the accuracy difference of the current channels, which should be less than 0.2%, but, some headroom should be left for possible transition effect, due to accidental synchronism of load current change at the rate of energy sampling.

Tamper circuit works if energies associated with the two current channels are both positive or negative, if two energies have different sign, a warning flag "TAMPER OR WRONG" in **DSP\_SR1** or **DSP\_SR2** is set.

The channel with higher energy is signaled by PHx TAMPER status bit in **DSP\_SR1** or **DSP\_SR2**.

When internal signals are not good enough to perform the calculations, for example line period is out or range or sigma-delta signals from analog section are stuck at high or low logic level, the tamper module is disabled and its state is set to normal.



## **8.4.11 AH accumulation**

In this particular tamper, the neutral wire is disconnected from the meter and the STPM3x does not sense the voltage anymore, while it keeps sensing the current information. In these conditions, AH accumulator can be used by the microcontroller to regularly calculate the billing based on a nominal voltage value due to the following equation:

## **Equation 18**

 $Energy = AH_ACC[31:0]·LSB<sub>IRMS</sub>·V<sub>NOM</sub>[Wh]$ 

If voltage is too low (sag event detected) or period is wrong (PER\_ERR = 1) and RMS value of current is high enough, energy is not cumulated but RMS current is accumulated in the register AH\_ACC[31:0]. Value in PHx AH\_ACC[31:0] register is increased with a *DCLK*  frequency.



The accumulation of current values is controlled by AH status bit. AH bit is set when PER\_ERR = 1 and real values of current overcome an upper threshold set in AH\_UPx[11:0] in **DSP\_CR9** and **DSP\_CR11**. This bit is cleared when RMS current drops below AH\_DOWNx[11:0] threshold in **DSP\_CR1**0 and **DSP\_CR12**.







<b>Parameter</b>	<b>Value</b>		
AH accumulator register LSB	$LSB_{AH \, ACC} = LSB_{I \, RMS}$ $2^{5}[Ah]$		
AH threshold register LSB	$LSB_{AH~UP} = LSB_{AH~DOWN} = LSB_{I~RMS} \cdot 2^{3}[A]$		

**Table 20. AH accumulator LSB**

# **8.4.12 Status bits, event bits and interrupt masks**

The device detects and monitors events like sag and swell, tamper, energy register overflow, power sign change, errors and generates an interrupt signal on INTx pins when the masked event is triggered.

Based on a certain event, the correspondent bit is set in two registers:

- Live event register
- Status (also called interrupt) register

While the interrupt is masked:

• Interrupt control mask register

## **Live event register**

In live event registers (**DSP\_EV1** and **DSP\_EV2**), events are set and cleared by DSP at the sampling rate *DCLK* = 7,8125 kHz.





Bit	Internal signal	<b>Description</b>
0		Sign total change active power
1	PH1+PH2 events <sup>(1)</sup>	Sign total change reactive power
$\overline{2}$		Overflow total active energy
3		Overflow total reactive energy
4		Sign change active power
5		Sign change active fundamental power
6		Sign change reactive power
7	PH <sub>x</sub> events	
8		Overflow active energy
9		Overflow active fundamental energy
10		Overflow reactive energy
11		
12		Current zero-crossing
13		Current sigma-delta bitstream stuck
14		<b>Current AH accumulation</b>
15	Cx events	
16		Current swell event history
17		
18		
19		Voltage zero-crossing
20		Voltage sigma-delta bitstream stuck
21		Voltage period error (out of range)
22		
23		Voltage swell event history
24	V <sub>x</sub> events	
25		
26		
27		Voltage sag event history
28		
29		
30		Reserved
31		Reserved

**Table 21. Live events**

1. Valid for the STPM33 and STPM34 only.



## **Status interrupt register**

DSP sets the status register (**DSP\_SR1** and **DSP\_SR2**) bits and they remain latched, even if the event ceases, until they are cleared to zero by a write operation.









#### **Table 22. Status register (continued)**

1. Valid for the STPM33 and STPM34 only.

## **Interrupt control mask register**

Each bit in the status register has a correspondent bit in **DSP\_IRQ1**, **DSP\_IRQ2** interrupt mask registers. If it set it outputs the correspondent status bit on INT1, INT2 pins respectively. In the STPM32, **DSP\_IRQ1** is mapped on INT1 pin only.

Status bits can be monitored by an external microcontroller application, in fact when INTx pin triggers, the application reads the relative status register content and clears it.

# **8.5 Functional description of communication peripheral**

The STPM3x can be interfaced to a control unit through a programmable communication peripheral which can be:

- 4-pin SPI
- 2-pin UART

The serial communication peripherals share same pins so that they cannot be used at the same time.

Interface selection is implemented through an internal detection system that, at the device startup, detects which of the two communication interfaces has to be used. This feature allows communication to be quickly established with minimal initialization.

Auto-detection works at startup by monitoring SCS pin status and automatically selecting the communication interface that matches the configuration:

- If SCS pin is held low the communication method is SPI
- If SCS pin is held high the communication interface is UART

After the selected communication interface is established, the interface is locked to prevent the communication method from changes, and SCS pin is used as chip-select for the device. The STPM3x locks automatically after the first successful communication.

Pins used by the serial communication peripheral are listed in *[Table 23](#page-62-0)*:

<span id="page-62-0"></span>





# **8.6 Communication protocol**

A single communication session consists of 4+1 (optional CRC) bytes full-duplex data sequence organized as follows:

<span id="page-63-0"></span>

<b>Byte</b>	Master-side transmitted data	Slave-side transmitted data	
	ADDRESS for 32-bit register to be read	Previously requested data byte LSB	
$\mathcal{P}$	ADDRESS for 16-bit register to be written   Previously requested data byte 2 out of 4		
3	DATA for 16-bit register to be written, LSB   Previously requested data byte 3 out of 4		
4	DATA for 16-bit register to be written, MSB   Previously requested data byte MSB		
5 (optional)	Master CRC verification packet	Slave CRC verification packet	

**Table 24. Communication session structures**

The above information is exchanged between master and slave in the same communication session, or transaction. SPI master can issue a read-request and a write-request (optional).

The master initiates the communication sending the STPM3x a frame see *[Table 24](#page-63-0)* (read address - write address - LS data byte - MS data byte - optional CRC).

Two command codes are provided:

- Dummy read address 0xFF increments by one the internal read pointer
- Dummy write address 0xFF specifies that no writing is requested (the two following incoming data frames are ignored)

Upon the reception of a frame, the STPM3x replies to master data sending the 32-bit register addressed during the previous communication session; during the first session the slave sends, by default, the 32-bit data stored into the first (row 0) memory register. Data are organized in 8-bit packets so that the least significant byte is sent first and the most significant byte is sent last.

A final 8-bit CRC packet is sent to master to verify no data corruption has occurred during the transmission from slave to master. The CRC feature, enabled by default, can be controlled by a configuration bit into US\_REG1 memory row (read address 0x24, write address 0x24).

If CRC bit in US\_REG1 is cleared, the communication consists of 4 bytes only.

Write-requests are executed immediately after the transaction has completed, while readrequests are fulfilled at the end of the next transaction only, because the sent read-address has just set the internal register pointer to deliver data during the following transaction.

So, while one transaction is enough to write data into memory, at least two transactions are needed to read selected data from memory.

Data bytes are swapped with respect to the order of the byte, since during transmission, the  $3<sup>rd</sup>$  byte sent to MOSI line is the least-significant (LS) byte (bits [7:0]) and the 4<sup>th</sup> byte is the most-significant (MS) byte of the data to be written (bits [15:8]).

On MISO line, the first data byte received is the least-significant (LS, bits [7:0]) and the last is the most-significant (MS, bits [31:24]) of the record, as shown below.





**Figure 43. Single communication time frame**

Data and configuration registers are organized into 32-bit rows in the internal memory, but can only be accessed 16-bit at a time for writing operations.

The address space is 70 rows wide, so there are 70 32-bit addressable elements for reading operations; since the first 21 configuration registers are writable, there are 42 (=21x2) 16-bit addressable elements for writing operations.

			32 bits 16 bits		
	MS Data [15:8]	LS Data [7:0]	<b>MS Data [15:8]</b>	LS Data $[7:0]$	<b>Write Address</b>
<b>Read Address</b> زبا	Data [31:24]	Data [23:16]	Data [15:8]	Data [7:0]	
	Data [31:24]	Data [23:16]	Data [15:8]	Data [7:0]	
	Data [31:24]	Data [23:16]	Data [15:8]	Data [7:0]	
					GIPG280320141430FSR

**Figure 44. Memory data organization**

Two different codes are used for the read address space and write address space, which can be found in the register map.

## **8.6.1 Synchronization and remote reset functionality**

Data into read-only registers are updated internally by DSP with frequency: 7,8125 kHz (clock frequency measure). Latching is used to sample the updated results into transmission latches. The transmission latches are flip-flops holding the data in the communication interface.

Data latching can be implemented in three ways:

- Using SYN and SCS pin
- Writing the channel latch bits before each reading (S/W Latchx in **DSP\_CR3**)
- Writing auto-latch bit (S/W Auto Latch in **DSP\_CR3**) to automatically latch data registers every clock measure period

The remote reset can be performed in two ways:

- Using SYN and SCS pin
- Writing the reset bit (S/W reset in **DSP\_CR3**)



## **SYN pin: latching, reset and global reset**

Latching of internal memory registers can be carried out by producing pulses of a given width on SYN pin while SCS line is high as depicted in *[Figure 45](#page-65-0)*.

If a single pulse on SYN is detected, latch occurs.

If two consecutive pulses are detected, a reset of measurement registers occurs and the counters are reset, as well.

If three consecutive pulses are detected, a global reset occurs, the configuration is also reset and the chip must be initialized again.

<span id="page-65-0"></span>



Latch pulse width and other SPI timings are reported in *[Table 5](#page-15-0)*.



**Figure 46. Latching through SYN pulses**

## **Software latch**

Writing S/W Latchx configuration bits of **DSP\_CR3** register can latch data into transmission latches. These two bits latch channel 1 and channel 2 data registers respectively; once set, they latch data and are automatically reset. By setting S/W Auto Latch bit, latching is performed automatically at the rate of sampling clock, so data latching, before each reading request, is no longer necessary.

# **8.6.2 SPI peripheral**

The device implements a full-duplex communication protocol using MISO, MOSI ports for data exchange, SCL for clock port, SCS port for data exchange activation and SYN for internal register data latching and resetting, when no data activation is set (SCS in off-state).



Latching and resetting can also be performed by setting the related bits in **DSP\_CR3** register.

With refernce to the general SPI protocol, the peripheral is configured to work according to the following settings: cpol=1, cpha=1.

#### **SPI control register**

**US\_REG1** register contains 16-bits with all the configuration parameters of t SPI and UART interfaces of the STPM3x.*[Table 25](#page-66-0)* describes SPI related bits:

<span id="page-66-0"></span>

<b>Bit position in</b> row	<b>Name</b>	<b>Description</b>	Default value
15	<b>LSBfirst</b>	Little(1) or $big(0)$ - endian for bit transmission in data-byte	
14	CRCenable	Enable/disable CRC feature	
[7:0]	CRCPolynomi a	Polynomial used to validate transmitted and received data	0x07

**Table 25. SPI control register**

LSBfirst: endianness of data-byte transmission and reception

CRCenable: enables the optional CRC feature

CRCPolynomial: default polynomial used is 0x07 (x8+x2+x+1)

#### **SPI timings**

Any single transaction timing follows the scheme in *[Figure 5](#page-11-0)*.

For consecutive writing transactions, a minimum time interval of 4 μs has to be taken into account in order to avoid overrun issues.

For latch and consecutive read transactions a minimum time interval of 4 μs has to be taken into account in order to avoid overrun issues.

#### **Examples**

All frames in the following examples do not contain CRC byte, which has to be added just in case the feature has not been disabled previously. After that CRC has been disabled, the frame consists of four bytes only.

To write bits from 31 to 16 (most significant bits) in row 1 with data byte 0xABCD and read row 2 in the following transaction, the first four bytes of the transmission (without CRC) are:

04\_03\_CD\_AB

To receive data from register 04 the master should send the frame:

FF\_FF\_FF\_FF

To write lower (least significant) 16-bits in row 3 with data #AABB and read back from the same row:

06\_06\_BB\_AA

And then



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## FF\_FF\_FF

To receive

The sent frame changes according to LSBfirst setting:



MISO line is valid as well. In this case, there is a full-reverse data transmission when LSBfirst=1, since data bit reception order changes as shown in the following table:

**Table 27. LSBfirst and MISO line**

	Byte[0]	Byte[1]	Byte[2]	Byte[3]
$LSBfirst = 0$	[7:0]	[15:8]	[23:16]	[31:24]
$LSBfirst = 1$	[0:7]	[8:15]	[16:23]	[24:31]

LSBfirst can be programmed using the transactions (other configuration bits involved in the transaction are set to their default states):

#### **Table 28. LSBfirst programming**



The transaction to write LSBfirst=0 is byte-reversed, since the system has moved from the LSBfirst=1 condition. The read address is set so to read in the following transaction the content of **US\_REG1**.

Following the frames to enable/disable CRC feature:

## **Table 29. CRCenable programming**



To reset status bits, the following frame should be sent:

28\_29\_00\_00

which resets all 16-bits (SPI and UART status registers). To clear SPI status bits only, SPImaster can send 1 s sequence to UART status bit register. Referring to the previous example, this leads to the following transaction:

28\_29\_FF\_00



Events are associated to interrupts so that, when the correspondent event mask bit in SPI IRQ register is activated, INT line is sensitive to that event.

For example, to activate CRC error interrupt (bit 12, related to status bit 28), the mask 0x1000 has to be written to write address 0x28 by the following transaction:

28\_28\_00\_10

## **8.6.3 UART peripheral**

The STPM3x provides the UART interface, which allows a communication using two singledirection pins only; this reduces the cost of isolated communication, where required, since two low cost opto-isolators are needed for this purpose.

Main features of this interface are:

- Full-duplex, asynchronous communication
- Low-level sequential data exchange protocol (1 start, 8 data, 1 stop)
- NRZ standard format (mark/space)
- Fractional baud rate generator system (to offer a wide range of baud rates)
- Several error detection flags
- Configurable frame length
- Optional configurable CRC checksum
- Optional noise immunity algorithm

TX pin accesses this interface, which transmits data to the microcontroller, and RX pin, which receives data from the microcontroller. A simple master/slave topology is implemented on the UART interface where the STPM3x acts as the slave.

Transmission and reception are driven by a common baud rate generator; the clock for each one is generated only when UART is enabled.

UART transmitting and receiving sections must have the same bit speed, frame length and stop bits.

Communication starts when the master sends slave a valid frame (the microcontroller). The format of the frame is shown below.



<span id="page-69-0"></span>

**Figure 47. UART frame**

As shown in *[Figure 47](#page-69-0)*, each frame consists of 10 bits. Each bit is sent to a variable rate. All frame data are sent LSBfirst.

If a BREAK frame is received, a break flag is set and the whole packet reception aborts.

The frame receiver can recognize an IDLE frame, but packet processing is not involved.

## **UART control register**

**US\_REG1** and **US\_REG2** registers respectively contain all the configuration parameters of SPI and UART interfaces of the STPM3x. *[Table 30](#page-69-1)* describes UART bits:

<span id="page-69-1"></span>

Row bit position	<b>Name</b>	<b>Description</b>	Default value
[23:16]	Timeout	Timeout threshold [ms]	
9	Break on error	Enable/disable the operation to send break frame in case of error	
8	Noise detection enable	Enable/disable error detection based on noise immunity algorithm	0
$[7:0]$	CRCPolynomial	Polynomial used to validate transmitted and received data	0x07

**Table 30. UART control register US\_REG1**

• Timeout: any communication session should be completed within this configurable time threshold (ms). If the timeout value is zero this threshold is disabled. If timeout expires, the reception and the transmission processes stop and, if enabled, a BREAK character is transmitted to warn the master about the error. Packet processing can resume only



after that BREAK transmission has been completed and an IDLE frame has been received.

- Break on error: if an error occurs (framing/noise/timeout/RX overrun) a BREAK command is transmitted to the master.
- Noise error detection. An oversampling technique is implemented to raise the noise level immunity: received bit value is accomplished taking in account the value of three samples, and applying to them the majority rule. This noise immunity algorithm is automatically enabled: if "noise detection enable" bit is set, all samples must have the same value to get a valid bit reception. In this case, when noise is detected within a frame, a noise detection error is issued and the whole packet is discarded.
- CRCPolynomial: default polynomial used is 0x07 (x8+x2+x+1).

CRC, in case of UART, has to be calculated on the reversed byte frame, because of the internal structure of UART blocks.

For example, if the frame to transmit is 04\_03\_CD\_AB, CRC should be calculated on the frame:

20\_C0\_B3\_D5 -> CRC = 0x16

The frame to send is: 04\_03 CD\_AB with the reversed CRC =  $68$ 

*Note: For UART peripheral, CRC byte is sent reversed only.*





- Frame delay: delay (expressed as bit periods) in transmitted frames. The bit period depends on the baud rate divider selection (see below).
- Baud rate: set to 9600 default value, the communication baud rate can be programmed in this configuration register. Theoretical values for configuration register can be calculated according to the following formulas, where a main clock frequency is 16 MHz, BR is the desired baud rate and BRDIV is the theoretical value of fractional divider:

## **Equation 19**

$$
BRDIV = \frac{Main \, Clock \, Frequency}{16 * Communication \,Baud \, Rate} = \frac{16 * 10^6}{16 * BR}
$$

## **Equation 20**

 $BRR_I = [BRDIV] = int(BRDIV)$ 

## **Equation 21**

 $BRR_F = round(16 * (BRDIV - BRR_I))$ 



where  $\mathsf{BR}_{\mathsf{I}}$  are bits [15:4] and  $\mathsf{BR}_{\mathsf{F}}$  are bits [3:0] of the register.

According to the chosen baud rate divider the bit period is:

## **Equation 22**

Bit Period =  $(16 * BR<sub>I</sub> + BR<sub>F</sub>) * MClk Period$ 

*[Table 32](#page-71-0)* summarizes the above calculation of the register value to select some typical baud rates:

<span id="page-71-0"></span>



# **8.6.4 UART/SPI status register and interrupt control register**

At row 20, at read address 0x28, the register is responsible for holding the status of UART/SPI peripherals of the STPM3x device. Setting the correspondent bit in IRQ CR the interrupt mask raises an interrupt on both INT1, INT2 pins based on the peripheral status.
Register	<b>Bit position</b>	<b>Description</b>	<b>Default value</b>	<b>Access</b> mode
	31	SPI busy	0	RO
	30	SPI RX overrun	0	<b>RW</b>
	29	SPI TX underrun	0	<b>RW</b>
	28	SPI CRC error	0	<b>RW</b>
	27	<b>UART/SPI write error</b>	0	<b>RW</b>
	26	<b>UART/SPI</b> read error	0	<b>RW</b>
	25	SPI TX empty	0	RO
<b>SR</b>	24	SPI RX full	0	<b>RO</b>
	22	<b>UART TX overrun</b>	0	<b>RW</b>
	21	<b>UART RX overrun</b>	0	<b>RW</b>
	20	<b>UART</b> noise error	0	<b>RW</b>
	19	<b>UART</b> frame error	0	<b>RW</b>
	18	<b>UART</b> timeout error	0	<b>RW</b>
	17	<b>UART CRC error</b>	0	<b>RW</b>
	16	<b>UART</b> break	0	<b>RW</b>
	15	mask for SPI busy status bit	0	<b>RW</b>
	14	mask for SPI RX overrun error status bit	0	<b>RW</b>
	13	mask for SPITX underrun error status bit	0	<b>RW</b>
	12	mask for SPI CRC error status bit	0	<b>RW</b>
	11	mask for write address error status bit	0	<b>RW</b>
	10	mask for read address error status bit	0	<b>RW</b>
<b>IRQ CR</b>	6	mask for UART TX overrun	0	<b>RW</b>
	5	mask for UART RX overrun	0	<b>RW</b>
	4	mask for UART noise error	0	<b>RW</b>
	3	mask for UART frame error	0	<b>RW</b>
	$\overline{c}$	mask for UART timeout error	0	<b>RW</b>
	$\mathbf{1}$	mask for UART CRC error	0	<b>RW</b>
	0	mask for UART break	0	<b>RW</b>

**Table 33. UART/SPI status and interrupt control register**

- SPI busy: peripheral in active state (for SPI diagnostic, not recommended for normal IRQ operations)
- SPI RX overrun: occurs when two consecutive write transactions are too fast and close to each other
- SPI TX underrun: occurs when a read-back operation (= write then read the same register) or latch/read is too fast



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- SPI CRC error: CRC error detected
- UART/SPI write error: write address out of range (not write address not writable)
- UART/SPI read error: read address out of range (not read address not readable)
- SPI TX empty: transmission buffer empty (for SPI diagnostic, not recommended for normal IRQ operations)
- SPI RX full: reception buffer full (for SPI diagnostic, not recommended for normal IRQ operations)
- UART TX overrun: occurs when master and slave have different baud rates and master transmits before reception has ended
- UART RX overrun: active when received data have not been correctly processed
- UART noise error: noisy bit detected
- UART frame error: missing stop bit detected
- UART timeout error: timeout counter expired
- UART CRC error: CRC error detected
- UART break: break frame (all zeros) received

Read-write status bits are set by the occurrence of the related event and are not reset when the event ceases, on contrary master can only reset them transmitting a write sequence addressed to memory location 0x28.



# **9 Application design and calibration**

The choice of external components in the transduction section of the application is a crucial point in the application design, affecting the precision and the resolution of the whole system. A compromise has to be found among the following needs:

- 1. Maximizing signal-to-noise ratio in the voltage and current channel
- 2. Choosing current-to-voltage conversion ratio  $k<sub>S</sub>$  and the voltage divider ratio in a way that calibration can be achieved for a given constant pulse  $C_P$
- 3. Choosing  $k<sub>S</sub>$  to take advantage of the whole current dynamic range according to desired maximum current and resolution

In this section, the rules for a good application design are described. After the design phase, any tolerance of the real components from these values or device internal parameter drift can be compensated through calibration.

Please refer to *[Section 8.4.6](#page-45-0)* and *[Section 8.4.7](#page-47-0)* for device basic calculations.

# <span id="page-74-0"></span>**9.1 Application design**

To reach  $C_P$  target output constant pulse, the analog front end component choice has to depend on:

- value of R1 voltage divider resistor, given R2 and  $k<sub>S</sub>$  current sensor sensitivity
- $-$  k<sub>S</sub> given R1 and R2 voltage divider resistors

Calculations for these two methods are developed below:

First method: constant  $k<sub>S</sub>$ 

Given R2 (smaller voltage divider resistor),  $k<sub>S</sub>$  (current sensor sensitivity) and the target meter constant pulse CP (pulses/kWh) as input of the calculations, the value of the voltage divider resistor R1 comes from the following formula:

# **Equation 23**

$$
R_1 = R_2 \left( \frac{1800 \cdot k_S \cdot A_V \cdot A_I \cdot cal_V \cdot cal_I \cdot DClk}{V_{ref}^2 \cdot C_P} - 1 \right) [\Omega]
$$

Second method: constant R1

Given R1, R2 (voltage divider resistors) and CP target meter constant pulse (pulses/kWh) as input of the calculations, the value of  $k<sub>S</sub>$  current sensor comes from the following formula:

# **Equation 24**

$$
k_{S} = \frac{V_{ref}^{2} \cdot C_{P} \cdot (1 + {R_{1}}_{R_{2}})}{1800 \cdot A_{V} \cdot A_{I} \cdot cal_{V} \cdot cal_{I} \cdot DClk} [mV/A]
$$

*Note: The resistor (the former) or the current channel sensor sensitivity (the latter) must be chosen as closer as possible to the target; small tolerance is compensated by the calibration, to reach the target constant pulse C<sub>P</sub>* 



With the above external components, the maximum measurable values of RMS voltage and current are:

#### **Equation 25**

$$
V_{MAX} = \frac{1}{2} \cdot \frac{V_{ref}}{A_V \cdot \sqrt{2}} \cdot \frac{R_1 + R_2}{R_2} [V]
$$

## **Equation 26**

$$
I_{MAX} = \frac{1}{2} \cdot \frac{V_{ref}}{A_I \cdot \sqrt{2}} \cdot \frac{1}{k_S} [A]
$$

These values are calculated leaving some available room for the input range with the peak value and minimizing modulator distortions.

The current resolution value is:

# **Equation 27**

$$
I_{MIN} = \frac{I_N}{X_I} = \frac{V_{ref}}{\sqrt{2} \cdot A_I \cdot k_{RMS} \cdot k_{int} \cdot k_S \cdot 2^{15}} [A]
$$

# **9.1.1 Example: current transformer case**

This example shows the correct dimensioning of a meter using a current transformer having the following specification:



## **Table 34. Example 1 design data**

The dimension of the voltage channel considers the voltage divider resistor values as 770 k $\Omega$  and 470 $\Omega$ .

Setting  $C_P = 64000$  pulses/kWh (at  $LPWX = 1$  - device default value) and according to calculation above the following values are:







To set the desired LED pulse output, a division factor can be set through LPWx[3:0] bits in **DSP\_CR1** and **DSP\_CR2** configuration registers.







<b>LPW<sub>x</sub></b>	<b>Division</b> factor	$C_{\rm P}$ [imp/kWh]	<b>LED</b> at $P_{\text{Nom}}$ [Hz]	<b>Pulse value</b> [Ws]	LSB <sub>P</sub> mW/LSB	LSB <sub>F</sub> mWs/LSB		
0111	8	8000	2,56	450	6,563	1,721		
1000	16	4000	1,28	900	13,127	3,441		
1001	32	2000	0.64	1800	26,253	6,882		
1010	64	1000	0,32	3600	52,507	13,764		
1011	128	500	0,16	7200	105,014	27,529		
1100	256	250	0.08	14400	210,028	55,057		
1101	512	125	0,04	28800	420,055	110,115		
1110	1024	62,5	0,02	57600	840.110	220,230		
1111	2048	31,25	0,01	115200	1680,221	440,460		

Table 36. LPWx bits, Cp. LSB<sub>p</sub> and LSB<sub>F</sub> relationships (continued)

The closer value to desired  $C_P$  is given by setting  $LPWX$  divider to 1010.

Any tolerance producing small variation of CP from 1000 imp/kWh can be compensated by calibration: setting CHV and CHI bits.

For a 1000 imp/kWh meter with these settings  $LSB_F=13.764$  mWs/LSB.

# **9.2 Application calibration**

The meter has to be calibrated so to compensate external component tolerances and internal  $V_{RFF}$  possible drift.

After the calibration, a meter using the STPM3x can reach IEC class 0.2 accuracy, taking into account that the component choice follows the rules explained above, and the layout and signal routing minimize the noise capture.

# **9.2.1 Voltage and current calibration (CHVx, CHIx bits)**

Thanks to the device internal architecture and linearity, all calculated values (RMS, energies and power) can be calibrated in a single point, just calibrating voltage and current streams.

For this purpose, a known nominal voltage  $V_N$  and current  $I_N$  must be applied to the meter under calibration.

Referring to *[Section 9.1](#page-74-0)* and *[Section 5](#page-20-0)*, having  $R_1$  or  $k<sub>S</sub>$  calculated as stated in the previous section, the target values of voltage and current RMS registers,  $\mathsf{X}_{\mathsf{V}}$  and  $\mathsf{X}_{\mathsf{I}}$  respectively are calculated as follows:







*Note:* For the above calculation, the calculated value of the component  $k<sub>S</sub>$  or  $R<sub>1</sub>$  (according to the *chosen design method) must be used; the difference of the real component is compensated by calibration as a tolerance.*

> To start calibration, the device has to be programmed with the proper gain and current sensor; moreover, to obtain the greatest correction dynamic, calibrators are initially set in the middle of their range (0x800), thus obtaining a calibration range of  $\pm$ 12.5% per voltage or current channel.

> After applying  $V_N$  and current  $I_N$  to the meter, a certain number of voltage and current RMS samples must be read and averaged (please, refer to averaged register values as  $V_{AV}$  and  $I_{AV}$ ) to calculate voltage and channel calibrators as follows:



#### **Table 38. Calibrator calculation**

The above procedure must be repeated for all voltage/current channels.

# **9.2.2 Phase calibration (PHVx, PHCx bits)**

The STPM3x does not introduce any phase shift between voltage and current channels.

However, the voltage and current signals come from transducers, which could have inherent phase errors. For example, a phase error of 0.1 ° to 0.3 ° is not uncommon for a current transformer (CT). These phase errors can vary from part to part, and they must be corrected in order to perform accurate power calculations. The errors associated with phase mismatch are particularly noticeable at low power factors.

The phase compensation block provides a method of digital phase correction of the phase shifting between voltage and current channels which can be introduced by the external component intrinsic characteristics or by external component mismatch. The amount of



phase compensation can be set per each channel, and it is executed delaying the currents and voltage samples using bits of the phase calibration configurators: PHCx[9:0] and PHVx[1:0].

These registers act in the same way by delaying the desired waveform by a certain quantity given from the equations below in degree:





A capacitive behavior is determined by the current leading the voltage waveform to a certain angle. In this case, there is the compensation by delaying the current waveform by the same angle through PHCx register. For a 50 Hz line the current channel waveform maximum delayed is:

 $\varphi_C \leq 4.6080^\circ$  with step  $\Delta \varphi_C = 0.0045^\circ$ 

An inductive behavior has the opposite effect, so that current lags the voltage waveform. In this case, PHV register delays the voltage waveform by the minimum angle to invert the behavior to capacitive and then acting on PHCx register for the fine tuning of the current waveform.

PHV impacts on the calculation of power and energies related to both current channels. For a 50 Hz line, the voltage channel waveform maximum delayed is:

 $\varphi_V \leq 6.912$  ° with step  $\Delta \varphi_V = 2.304$  °.



#### **Figure 48. Phase shift error**



The Θ angle can be measured through the error on active power (from LED) averaged over a certain number of samples (i.e. 50) at power factor  $PF = 0.5$ .

For example, if the error  $=$  e, the phase shift between voltage and current is:

# **Equation 28**

$$
\theta = \cos^{-1}\left(\frac{1-e}{2}\right) - 60^{\circ}
$$

To compensate this error, PHC and PHV bits must be set as below, to introduce a correction factor φ=-Θ













# **9.2.3 Power offset calibration (OFAx, OFAFx, OFRx, OFSx bits)**

The device has the power offset compensation register for all measured powers (active, active fundamental, reactive and apparent) to compensate, for each channel, the power measured due to noise capture in the application.

Power registers are signed values, (MSB is the sign and negative values are two's complemented); the power offset registers are also signed registers with LSB value equal to 4 times the power LSB:





Power offset can be compensated by measuring the power value when the current  $I = 0$ , if the average value is not null; the value is due to external influences, then an opposite value should be applied to the power offset register.



# **10 Register map**

There are three types of data register:

- RW: read and written by application (in orange in the picture below)
- RWL: the status bits, set from DSP, must be latched to read updated content, and must be cleared by the application (in orange in the picture below)
- RL: read registers only, they contain measured data and are continuously updated by DSP, so they need to be latched before reading (in blue in the picture below)

The following nomenclature is used in the above registers:

- A: active wideband
- F: active fundamental
- R: reactive
- S: apparent



# **10.1 Register map graphical representation**



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STPM32, STPM33, STPM34 **STPM32, STPM33, STPM34 Register map**

Register map

 $\overline{\mathbf{A}}$ 





STPM32, STPM33, STPM34 **STPM32, STPM33, STPM34 Register map**

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Register map



 $\overline{\mathbf{A}}$ 



STPM32, STPM33, STPM34 **STPM32, STPM33, STPM34 Register map**

Register map



 $\overline{\mathbf{A}}$ 



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 $\overline{\mathbf{A}}$ 



STPM32, STPM33, STPM34 **STPM32, STPM33, STPM34 Register map**

Register map





STPM32, STPM33, STPM34 **STPM32, STPM33, STPM34 Register map**

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Register map



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AlF RIS

# **10.2 Configuration register**

Row	<b>Bit</b>	Internal signal	<b>Description</b>	<b>Default</b>
	0			0
	1	CLRSS_TO1	Set duration of primary channel signal to clear sag and swell	$\Omega$
	2		and avoid race condition on digital counters	$\Omega$
	3			$\Omega$
	4	ClearSS1	Clear sag and swell time register and history bits for primary channel, auto-reset to '0'	0
	5	ENVREF1	Enable internal voltage reference for primary channel: 0: reference disabled – external $V_{REF}$ required 1: reference enabled	1
	6			$\Omega$
0	$\overline{7}$	TC <sub>1</sub>	Temperature compensation coefficient selection for primary channel voltage reference V <sub>RFF1</sub> (See Table 9)	1
	8			$\mathbf 0$
	9		Reserved	$\mathbf 0$
	10		Reserved	0
	11		Reserved	$\mathbf 0$
	12		Reserved	$\mathbf 0$
	13		Reserved	$\Omega$
	14		Reserved	$\Omega$
	15		Reserved	$\Omega$
	16		Reserved	$\Omega$

**Table 44. DSP control register 1 (DSP\_CR1)**



Row	<b>Bit</b>	<b>Internal signal</b>	<b>Description</b>	<b>Default</b>
0	17	AEM1	Apparent energy mode for primary channel: 0: use apparent RMS power 1: use apparent vectorial power	
	18	APM1	Apparent vectorial power mode for primary channel: 0: use fundamental power 1: use active power	
	19	BHPFV1	Bypass hi-pass filter for primary voltage channel: 0: HPF enabled 1: HPF bypassed	
	20	BHPFC1	Bypass hi-pass filter for primary current channel: 0: HPF enabled 1: HPF bypassed	
	21	ROC <sub>1</sub>	Add Rogowski integrator to primary current channel filtering pipeline: 0: integrator bypassed 1: integrator enabled	
	22	BLPFV1	Primary voltage channel frequency content used for reactive power calculation: 0: fundamental 1: wideband	
	23	BLPFC1	Primary current channel frequency content used for reactive power calculation: 0: fundamental 1: wideband	
	24			
	25		LED1 speed dividing factor: $0x0 = 2$ $(-4)$ , $0xF = 2$ $11$	
	26	LPW1	Default $0x4 = 1$	
	27			
	28		LED1 pulse-out power selection:	
	29	LPS1	LPS1 [1:0]: 00,01,10,11 LED1 output: active, fundamental, reactive, apparent	
	30		LED1 pulse-out channel selection:	
	31	LCS <sub>1</sub>	LCS1 [1:0]: 00,01,10,11 LED1: primary channels, secondary channels, algebraic, sigma-delta bitstream	

**Table 44. DSP control register 1 (DSP\_CR1) (continued)**



<b>Row</b>	<b>Bit</b>	Internal signal	<b>Description</b>	<b>Default</b>
	0			0
	1	CLRSS_TO2	Set duration of secondary channel signal to clear sag and	$\Omega$
	2		swell and avoid race condition on digital counters	$\Omega$
	3			$\Omega$
	4	ClearSS2	Clear sag and swell time register and history bits for primary channel, auto-reset to 0	$\Omega$
1	5	ENVREF2	Enable internal voltage reference for primary channel: 0: reference disabled – external $V_{REF}$ required 1: reference enabled	1
	6	TC <sub>2</sub>	Temperature compensation coefficient selection for primary channel voltage reference V <sub>REF2</sub> . (See Table 9)	$\Omega$
	$\overline{7}$			1
	8			$\Omega$
	9		Reserved	$\Omega$
	10		Reserved	$\Omega$
	11		Reserved	$\Omega$
	12		Reserved	$\Omega$
	13		Reserved	$\Omega$
	14		Reserved	$\Omega$
	15		Reserved	$\Omega$
	16		Reserved	0

**Table 45. DSP control register 2 (DSP\_CR2)**



Row	<b>Bit</b>	<b>Internal signal</b>	<b>Description</b>	<b>Default</b>
	17	AEM2	Apparent energy mode for primary channel: 0: use apparent RMS power 1: use apparent vectorial power	
	18	APM <sub>2</sub>	Apparent vectorial power mode for primary channel: 0: use fundamental power 1: use active power	
	19	BHPFV2	Bypass hi-pass filter for primary voltage channel: 0: HPF enabled 1: HPF bypassed	
1	20	BHPFC2	Bypass hi-pass filter for primary current channel: 0: HPF enabled 1: HPF bypassed	
	21	ROC <sub>2</sub>	Add Rogowski integrator to primary current channel filtering pipeline: 0: integrator bypassed 1: integrator enabled	
	22	BLPFV <sub>2</sub>	Primary voltage channel frequency content used for reactive power calculation: 0: fundamental 1: wideband	
	23	BLPFC <sub>2</sub>	Primary current channel frequency content used for reactive power calculation: 0: fundamental 1: wideband	
	24			
	25		LED2 speed dividing factor: $0x0 = 2$ $(-4)$ , $0xF = 2$ $11$	
	26	LPW <sub>2</sub>	Default $0x4 = 1$	
	27			
	28		LED2 pulse-out power selection:	
	29	LPS <sub>2</sub>	LPS2 [1:0]: 00,01,10,11 LED2: output, active, fundamental, reactive, apparent	
	30		LED2 pulse-out channel selection:	
	31	LCS <sub>2</sub>	LCS2 [1:0]: 00,01,10,11 LED2: primary channels, secondary channels, algebraic, sigma-delta bitstream	

**Table 45. DSP control register 2 (DSP\_CR2) (continued)**



Row	<b>Bit</b>	<b>Internal signal</b>	<b>Description</b>	<b>Default</b>
	0			$\mathbf 0$
	$\mathbf{1}$			$\mathbf 0$
	$\overline{c}$			$\mathbf 0$
	3			$\mathbf 0$
	$\overline{4}$			$\mathbf 0$
	5			$\mathbf{1}$
	6	TIME_VALUE	Time counter threshold for voltage sag detection	1
	$\overline{7}$			1
	8			$\mathbf 0$
2	9			$\mathbf 0$
	10			$\mathbf{1}$
	11			$\mathbf 0$
	12			$\mathbf 0$
	13			$\mathbf 0$
	14		Selection bit for ZCR/CLK pin, (output depends on ZCR/CLK enable bit):	$\Omega$
	15	ZCR_SEL	ZCR_SEL[1:0]: 00, 01, 10, 11 ZCR: V1, C1, V2, C2 CLK: 7.8125 kHz, 4 MHz, 4 MHz, 50% duty cycle, 16 MHz	$\mathbf 0$
	16	ZCR_EN	ZCR/CLK pin output: 0:CLK 1:ZCR	$\mathbf 0$

**Table 46. DSP control register 3 (DSP\_CR3)**



Row	<b>Bit</b>	<b>Internal signal</b>	<b>Description</b>	<b>Default</b>
	17 18	TMP_TOL	Selection bits for tamper tolerance: TMP_TOL[1:0]: 00, 01, 10, 11 Tolerance: 12.5%, 8.33%, 6.25%, 3.125%	0 0
2	19	TMP_EN	Enable tampering feature: 0: tamper disable 1: tamper enable	0
	20	S/W Reset	Global reset brings the entire register map to default This bit is set to zero after this action automatically	$\Omega$
	21	S/W Latch1	Primary channel measurement register latch This bit is set to zero after this action automatically	0
	22	S/W Latch2	Secondary channel measurement register latch his bit is set to zero after this action automatically	0
	23	S/W Auto Latch	Automatic measurement register latch at 7.8125 kHz	0
	24	LED1OFF	LED1 pin output disable 0: LED1 output on 1: LED1 output disabled When the LED output is disabled the pin is set at low-state	0
	25	LED2OFF	LED2 pin output disable 0: LED2 output on 1: LED2 output disabled When the LED output is disabled the pin is set at low-state	0
	26	EN_CUM	Cumulative energy calculation 0: cumulative is the sum of channel energies 1: total is the difference of energies	0
	27	REF_FREQ	Reference line frequency: $0:50$ Hz $1:60$ Hz	0
	28		Reserved	0
	29		Reserved	0
	30		Reserved	0
	31		Reserved	0

**Table 46. DSP control register 3 (DSP\_CR3) (continued)**



Row	<b>Bit</b>	<b>Internal signal</b>	<b>Description</b>	<b>Default</b>
	$\pmb{0}$			0
	1			0
	$\overline{c}$			0
	3			0
	$\overline{\mathbf{4}}$	PHC <sub>2</sub>	Secondary current channel phase compensation	0
	5		register	0
	6			0
	$\overline{7}$			0
	8			0
	9			0
	10	PHV <sub>2</sub>	Secondary voltage channel phase compensation	0
	11		register	$\pmb{0}$
	12		Primary current channel phase compensation register	0
	13			0
3	14	PHC1		0
	15			0
	16			0
	17			0
	18			0
	19			0
	20			$\mathsf 0$
	21			0
	22	PHV1	Primary voltage channel phase compensation register	0
	23			$\pmb{0}$
	24		Reserved	0
	25		Reserved	0
	26		Reserved	$\mathsf 0$
	27		Reserved	0
	28		Reserved	0
	29		Reserved	0
	30		Reserved	$\pmb{0}$
	31		Reserved	0

**Table 47. DSP control register 4 (DSP\_CR4)**



Row	<b>Bit</b>	<b>Internal signal</b>	<b>Description</b>	<b>Default</b>	
	0			0	
	$\mathbf{1}$			$\pmb{0}$	
	$\boldsymbol{2}$			$\mathbf 0$	
	3			$\mathbf 0$	
	$\overline{4}$			$\pmb{0}$	
	5	CHV1	Calibration register of primary voltage channel	$\pmb{0}$	
	$\,6\,$			$\mathbf 0$	
	$\boldsymbol{7}$			$\pmb{0}$	
	8			$\mathbf 0$	
	$\boldsymbol{9}$			$\mathsf 0$	
	10			$\mathsf 0$	
	11			$\mathbf{1}$	
	12	SWV_THR1	Swell threshold of primary voltage channel	$\mathbf{1}$	
	13			$\mathbf{1}$	
	14			$\mathbf{1}$	
$\overline{\mathbf{4}}$	15			$\mathbf{1}$	
	$16\,$			$\mathbf{1}$	
	17			$\mathbf{1}$	
	18			$\mathbf{1}$	
	19			$\mathbf{1}$	
	$20\,$			$\mathbf{1}$	
	21			$\mathbf{1}$	
	22			$\pmb{0}$	
	23			$\pmb{0}$	
	24			$\pmb{0}$	
	25			0	
	26	SAG_THR1	Sag threshold of primary voltage channel	$\pmb{0}$	
	27			$\pmb{0}$	
	28			$\pmb{0}$	
	29			$\pmb{0}$	
	$30\,$			$\pmb{0}$	
	31				$\mathbf 0$

**Table 48. DSP control register 5 (DSP\_CR5)**





**Table 49. DSP control register 6 (DSP\_CR6)**



Row	<b>Bit</b>	<b>Internal signal</b>	<b>Description</b>	<b>Default</b>
	$\pmb{0}$			$\pmb{0}$
	$\mathbf{1}$		Calibration register of secondary voltage channel	$\pmb{0}$
	$\boldsymbol{2}$			$\pmb{0}$
	$\sqrt{3}$			$\pmb{0}$
	$\overline{4}$	CHV <sub>2</sub>		$\pmb{0}$
	5			$\pmb{0}$
	$\,6$			$\pmb{0}$
	$\overline{7}$			$\pmb{0}$
	8			$\pmb{0}$
	$\boldsymbol{9}$			$\pmb{0}$
	10			$\pmb{0}$
	11			$\mathbf{1}$
	12	SWV_THR2	Swell threshold of secondary voltage channel	$\mathbf{1}$
	13			$\mathbf{1}$
	14			$\mathbf{1}$
$\,6$	15			$\mathbf{1}$
	16			$\mathbf{1}$
	17			$\mathbf{1}$
	18			$\mathbf{1}$
	19			$\mathbf{1}$
	20			$\mathbf{1}$
	21			$\mathbf{1}$
	22	SAG_THR2	Sag threshold of secondary voltage channel	$\pmb{0}$
	23			$\pmb{0}$
	24			$\pmb{0}$
	25			$\pmb{0}$
	26			$\pmb{0}$
	27			$\pmb{0}$
	28			$\pmb{0}$
	29			$\pmb{0}$
	$30\,$			$\mathbf 0$
	31			$\pmb{0}$

**Table 50. DSP control register 7 (DSP\_CR7)**



Row	<b>Bit</b>	<b>Internal signal</b>	<b>Description</b>	<b>Default</b>
	$\pmb{0}$			$\,0\,$
	$\mathbf 1$			$\,0\,$
	$\overline{c}$			$\pmb{0}$
	$\ensuremath{\mathsf{3}}$			$\pmb{0}$
	$\overline{\mathbf{4}}$			$\pmb{0}$
	5	CHC <sub>2</sub>		$\pmb{0}$
	$\,6$		Calibration register of secondary current channel	$\mathbf 0$
	$\overline{7}$			$\pmb{0}$
	8			$\pmb{0}$
	9			$\pmb{0}$
	10			$\pmb{0}$
	11			$\mathbf{1}$
	12		Swell threshold of secondary current channel	$\mathbf{1}$
	13			$\mathbf{1}$
	14	SWC_THR2		$\mathbf{1}$
	15			$\mathbf{1}$
$\overline{7}$	16			$\mathbf{1}$
	17			$\mathbf{1}$
	18			$\mathbf{1}$
	19			$\mathbf{1}$
	20			$\mathbf{1}$
	21			$\mathbf{1}$
	22		Reserved	$\mathsf 0$
	23		Reserved	$\pmb{0}$
	24		Reserved	$\pmb{0}$
	25		Reserved	$\pmb{0}$
	26		Reserved	$\pmb{0}$
	27		Reserved	$\pmb{0}$
	28		Reserved	$\mathsf 0$
	29		Reserved	$\pmb{0}$
	30		Reserved	$\pmb{0}$
	31		Reserved	$\pmb{0}$

**Table 51. DSP control register 8 (DSP\_CR8)**


Row	<b>Bit</b>	<b>Internal signal</b>	<b>Description</b>	<b>Default</b>
	0			$\mathbf{1}$
	$\mathbf{1}$			$\mathbf{1}$
	$\overline{c}$			$\mathbf{1}$
	$\ensuremath{\mathsf{3}}$			$\mathbf{1}$
	$\overline{\mathbf{4}}$			$\mathbf{1}$
	$\,$ 5 $\,$	AH_UP1	Primary channel RMS upper threshold (for AH)	$\mathbf{1}$
	6			$\mathbf{1}$
	$\overline{7}$			$\mathbf{1}$
	8			$\mathbf{1}$
	$\boldsymbol{9}$			$\mathbf{1}$
	$10$			$\mathbf{1}$
	11			$\mathbf{1}$
	12	OFA1	Offset for primary channel active power	$\mathbf 0$
	13			$\mathbf 0$
	14			$\mathsf 0$
8	15			$\mathbf 0$
	16			$\mathsf 0$
	17			$\mathsf{O}\xspace$
	18			$\pmb{0}$
	19			$\pmb{0}$
	$20\,$			$\mathsf 0$
	21			$\mathbf 0$
	22			$\mathbf 0$
	23			$\pmb{0}$
	24			$\,0\,$
	25			$\mathbf 0$
	26	OFAF1	Offset for primary channel fundamental active power	$\mathsf 0$
	27			$\mathbf 0$
	28			$\mathsf{O}\xspace$
	29			$\mathbf 0$
	$30\,$			$\pmb{0}$
	31			$\pmb{0}$

**Table 52. DSP control register 9 (DSP\_CR9)**



Row	<b>Bit</b>	<b>Internal signal</b>	<b>Description</b>	<b>Default</b>
	0			$\mathbf{1}$
	$\mathbf{1}$			$\mathbf{1}$
	$\overline{c}$			$\mathbf{1}$
	$\ensuremath{\mathsf{3}}$			$\mathbf{1}$
	$\overline{\mathbf{4}}$			$\mathbf{1}$
	$\,$ 5 $\,$	AH_DOWN1	Primary channel RMS lower threshold (for AH)	$\mathbf{1}$
	6			$\mathbf{1}$
	$\overline{7}$			$\mathbf{1}$
	$\bf 8$			$\mathbf{1}$
	9			$\mathbf{1}$
	$10$			$\mathbf{1}$
	11			$\mathbf{1}$
	12		Offset for primary channel reactive power	$\mathsf 0$
	13			$\mathbf 0$
	14			$\pmb{0}$
9	15			$\mathsf 0$
	16	OFR1		$\pmb{0}$
	17			$\pmb{0}$
	$18$			$\mathsf 0$
	19			$\pmb{0}$
	20			$\pmb{0}$
	21			$\mathsf 0$
	22			$\pmb{0}$
	23			0
	24			$\mathsf 0$
	25			$\mathbf 0$
	26	OFS1	Offset for primary channel apparent power	$\pmb{0}$
	27			$\mathsf 0$
	28			$\pmb{0}$
	29			$\pmb{0}$
	$30\,$			$\mathsf 0$
	31			$\mathbf 0$

**Table 53. DSP control register 10 (DSP\_CR10)**



Row	<b>Bit</b>	<b>Internal signal</b>	<b>Description</b>	<b>Default</b>
	$\pmb{0}$			$\mathbf{1}$
	$\mathbf{1}$			$\mathbf{1}$
	$\sqrt{2}$			$\mathbf{1}$
	3			$\mathbf{1}$
	4			$\mathbf{1}$
	5	AH_UP2	Secondary channel RMS upper threshold (for AH)	$\mathbf{1}$
	6			$\ddagger$
	$\overline{7}$			$\mathbf 1$
	8			$\mathbf{1}$
	$\boldsymbol{9}$			$\mathbf{1}$
	$10$			$\mathbf{1}$
	11			$\mathbf{1}$
	12	OFA <sub>2</sub>	Offset for secondary channel active power	$\mathbf 0$
	13			$\mathbf 0$
	14			0
10	15			$\mathbf 0$
	$16\,$			$\mathbf 0$
	$17\,$			$\pmb{0}$
	18			$\mathbf 0$
	19			$\pmb{0}$
	20			$\pmb{0}$
	21			$\mathbf 0$
	22			$\mathbf 0$
	23			0
	24			$\mathbf 0$
	25			$\pmb{0}$
	26	OFAF <sub>2</sub>	Offset for secondary channel fundamental active power	$\mathbf 0$
	$27\,$			$\mathbf 0$
	$28\,$			$\pmb{0}$
	29			$\mathsf 0$
	$30\,$			$\pmb{0}$
	31			$\mathbf 0$

**Table 54. DSP control register 11 (DSP\_CR11)**



Row	<b>Bit</b>	<b>Internal signal</b>	<b>Description</b>	<b>Default</b>
	$\pmb{0}$			$\mathbf{1}$
	$\mathbf{1}$			$\mathbf{1}$
	$\boldsymbol{2}$			$\mathbf{1}$
	3			$\mathbf{1}$
	$\overline{\mathbf{4}}$			$\mathbf{1}$
	5	AH_DOWN2	Secondary channel RMS lower threshold (for AH)	$\mathbf{1}$
	6			$\mathbf{1}$
	$\boldsymbol{7}$			$\mathbf{1}$
	8			$\mathbf{1}$
	$\boldsymbol{9}$			$\mathbf{1}$
	10			$\mathbf{1}$
	11			$\mathbf{1}$
	12	OFR <sub>2</sub>	Offset for secondary channel reactive power	$\mathbf 0$
	13			$\mathbf 0$
	14			$\pmb{0}$
11	15			$\boldsymbol{0}$
	$16\,$			$\pmb{0}$
	17			$\pmb{0}$
	18			$\mathbf 0$
	19			$\mathbf 0$
	20			$\mathbf 0$
	21			$\boldsymbol{0}$
	22			$\pmb{0}$
	23			$\pmb{0}$
	24			$\pmb{0}$
	25			$\mathbf 0$
	$26\,$	OFS <sub>2</sub>	Offset for secondary channel apparent power	$\pmb{0}$
	27			$\pmb{0}$
	28			$\pmb{0}$
	29			$\mathbf 0$
	$30\,$			$\pmb{0}$
	31			$\mathbf 0$

**Table 55. DSP control register 12 (DSP\_CR12)**



Row	<b>Bit</b>	Internal signal	<b>Description</b>	<b>Default</b>
	$\pmb{0}$		Reserved	$\mathbf{1}$
	$\mathbf{1}$		Reserved	$\mathbf{1}$
	2		Reserved	$\mathbf{1}$
	3		Reserved	0
	$\overline{\mathbf{4}}$		Reserved	$\pmb{0}$
	$\sqrt{5}$		Reserved	$\mathbf{1}$
	6		Reserved	$\,0\,$
	$\overline{7}$		Reserved	0
	8		Reserved	$\mathbf{1}$
	$\boldsymbol{9}$		Reserved	$\mathbf{1}$
	10		Reserved	$\pmb{0}$
	11		Reserved	$\pmb{0}$
	12		Reserved	$\mathbf 0$
	13		Reserved	$\pmb{0}$
	14		Reserved	$\pmb{0}$
	15		Reserved	$\mathbf 0$
12	16		Reserved	$\mathbf{1}$
	17		Reserved	$\mathbf{1}$
	18		Reserved	$\mathbf{1}$
	19		Reserved	$\pmb{0}$
	20		Reserved	$\pmb{0}$
	21		Reserved	$\mathbf{1}$
	22		Reserved	$\pmb{0}$
	23		Reserved	$\,0\,$
	24		Reserved	$\mathbf{1}$
	25		Reserved	$\mathbf{1}$
	26		Gain selection of primary current channel:	$\mathbf{1}$
	27	GAIN1	GAIN1[1:0]: 00, 01, 10, 11 GAIN: x2, x4, x8, x16	$\mathbf{1}$
	28		Reserved	$\mathbf 0$
	29		Reserved	$\pmb{0}$
	30		Reserved	0
	31		Reserved	$\pmb{0}$

**Table 56. Digital front end control register 1 (DFE\_CR1)**









Row	<b>Bit</b>	Internal signal	<b>Description</b>	<b>Default</b>
	0	<b>CUM IRQ CR</b>	Sign change total active power	0
	1		Sign change total reactive power	0
	2		Overflow total active energy	0
	3		Overflow total reactive energy	0
	4		Sign change secondary channel active power	0
	5		Sign change secondary channel active fundamental power	0
	6		Sign change secondary channel reactive power	0
	7	PH <sub>2</sub> IRQ CR	Sign change secondary channel apparent power	0
	8		Overflow secondary channel active energy	0
	9		Overflow secondary channel active fundamental energy	0
	10		Overflow secondary channel reactive energy	0
	11		Overflow secondary channel apparent energy	0
	12	PH1 IRQ CR	Sign change primary channel active power	$\mathbf 0$
	13		Sign change primary channel active fundamental power	0
14	14		Sign change primary channel reactive power	0
	15		Sign change primary channel apparent power	0
	16		Overflow primary channel active energy	0
	17		Overflow primary channel active fundamental energy	0
	18		Overflow primary channel reactive energy	0
	19		Overflow primary channel apparent energy	0
	20	C <sub>1</sub> IRQ CR	Primary current sigma-delta bitstream stuck	0
	21		AH1 - accumulation of primary channel current	0
	22		Primary current swell start	0
	23		Primary current swell end	0
	24		Primary voltage sigma-delta bitstream stuck	0
	25		Primary voltage period error	0
	26	V1 IRQ CR	Primary voltage sag start	0
	27		Primary voltage sag end	0
	28		Primary voltage swell start	0
	29		Primary voltage swell end	0
	30	Tamper	Tamper on primary	0
	31		Tamper or wrong connection	0

**Table 58. DSP interrupt control mask register 1 (DSP\_IRQ1)**







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<b>Row</b>	Bit	<b>Internal signal</b>	<b>Description</b>	<b>Default</b>
	0		Sign change total active power	0
	1	PH1+PH2 status	Sign change total reactive power	0
	$\overline{2}$		Overflow total active energy	0
	3		Overflow total reactive energy	0
	4		Sign change secondary channel active power	0
	5		Sign change secondary channel active fundamental power	0
	6		Sign change secondary channel reactive power	0
	7	PH <sub>2</sub> IRQ status	Sign change secondary channel apparent power	0
	8		Overflow secondary channel active energy	0
	9		Overflow secondary channel active fundamental energy	0
	10		Overflow secondary channel reactive energy	0
	11		Overflow secondary channel apparent energy	0
	12		Sign change primary channel active power	0
	13		Sign change primary channel active fundamental power	0
16	14		Sign change primary channel reactive power	0
	15	PH1 IRQ status	Sign change primary channel apparent power	0
	16		Overflow primary channel active energy	0
	17		Overflow primary channel active fundamental energy	0
	18		Overflow primary channel reactive energy	0
	19		Overflow primary channel apparent energy	0
	20	C1 IRQ status	Secondary current sigma-delta bitstream stuck	0
	21		AH1 - accumulation of secondary channel current	0
	22		Secondary current swell start	0
	23		Secondary current swell end	0
	24		Secondary voltage sigma-delta bitstream stuck	0
	25		Secondary voltage period error	0
	26	V1 IRQ status	Secondary voltage sag start	0
	27		Secondary voltage sag end	0
	28		Secondary voltage swell start	0
	29		Secondary voltage swell end	0
	30	Tamper	Tamper on secondary	0
	31		Tamper or wrong connection	0

**Table 60. DSP status register 1 (DSP\_SR1)**



Row	<b>Bit</b>	<b>Internal signal</b>	<b>Description</b>	<b>Default</b>
	0	PH1+PH2 status	Sign change total active power	0
	1		Sign change total reactive power	0
	$\overline{2}$		Overflow total active energy	0
	3		Overflow total reactive energy	0
	4		Sign change secondary channel active power	0
	5		Sign change secondary channel active fundamental power	0
	6		Sign change secondary channel reactive power	0
	7	PH <sub>2</sub> status	Sign change secondary channel apparent power	0
	8		Overflow secondary channel active energy	0
	9		Overflow secondary channel active fundamental energy	0
	10		Overflow secondary channel reactive energy	0
	11		Overflow secondary channel apparent energy	0
	12		Sign change primary channel active power	0
	13		Sign change primary channel active fundamental power	0
17	14		Sign change primary channel reactive power	0
	15	PH1 status	Sign change primary channel apparent power	0
	16		Overflow primary channel active energy	0
	17		Overflow primary channel active fundamental energy	0
	18		Overflow primary channel reactive energy	0
	19		Overflow primary channel apparent energy	0
	20		Secondary current sigma-delta bitstream stuck	0
	21	C <sub>2</sub> status	AH1 - accumulation of secondary channel current	0
	22		Secondary current swell start	0
	23		Secondary current swell end	0
	24		Secondary voltage sigma-delta bitstream stuck	0
	25		Secondary voltage period error	0
	26	V <sub>2</sub> status	Secondary voltage sag start	0
	27		Secondary voltage sag end	0
	28		Secondary voltage swell start	0
	29		Secondary voltage swell end	0
	30	Tamper	Tamper on secondary	0
	31		Tamper or wrong connection	0

**Table 61. DSP status register 2 (DSP\_SR2)**

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## **10.3 UART/SPI registers**









### **Table 63. UART/SPI control register 2 (US\_REG2)**



<b>Row</b>	Bit	Internal signal	<b>Description</b>	<b>Default</b>
	0	<b>UART</b> break	Activate IRQ on INT1, INT2 for selected signals	0
	1	<b>UART CRC error</b>	Activate IRQ on both INT1, INT2 for selected signals	0
	$\overline{2}$	<b>UART</b> timeout error	Activate IRQ on both INT1, INT2 for selected signals	0
	3	<b>UART</b> framing error	Activate IRQ on both INT1, INT2 for selected signals	0
	4	UART noise error	Activate IRQ on both INT1, INT2 for selected signals	0
	5	<b>UART RX overrun</b>	Activate IRQ on both INT1, INT2 for selected signals	0
	6	<b>UART TX overrun</b>	Activate IRQ on both INT1, INT2 for selected signals	0
	$\overline{7}$		Reserved	1
	8		Reserved	0
	9		Reserved	0
	10	UART/SPI read error	Activate IRQ on both INT1, INT2 for selected signals	0
	11	<b>UART/SPI write</b> error	Activate IRQ on both INT1, INT2 for selected signals	0
	12	SPI CRC error	Activate IRQ on both INT1, INT2 for selected signals	0
	13	SPI TX underrun	Activate IRQ on both INT1, INT2 for selected signals	0
20	14	SPI RX overrun	Activate IRQ on both INT1, INT2 for selected signals	0
	15		Reserved	0
	16	<b>UART</b> break	Break frame (all zeros) received	0
	17	<b>UART CRC error</b>	CRC error detected	0
	18	<b>UART</b> timeout error	Timeout counter expired	0
	19	<b>UART</b> framing error	Missing stop bit detected	0
	20	UART noise error	Noisy bit detected	0
	21	<b>UART RX overrun</b>	Active when received data have not been correctly processed	0
	22	<b>UART TX overrun</b>	Occurs when master and slave have different baud rates and master transmits before reception has ended	0
	23		Reserved	0
	24	SPI RX full	Reception buffer full (for SPI diagnostic, not recommended for normal IRQ operations)	0
	25	SPI TX empty	Transmission buffer empty (for SPI diagnostic, not recommended for normal IRQ operations)	0
	26	UART/SPI read error	Read address out of range (not readable)	0

**Table 64. UART/SPI control register 3 (US\_REG3)**



Row	Bit	Internal signal	<b>Description</b>	<b>Default</b>
20	27	<b>UART/SPI write</b> error	Write address out of range (NOT writable)	
	28	SPI CRC error	CRC error detected	
	29	SPI TX underrun	Occurs when a read-back operation (= write then read the same register) or latch $+$ read is too fast	0
	30	SPI RX overrun	Occurs when two consecutive write transactions are too fast and close to each other	0
	31		Reserved	

**Table 64. UART/SPI control register 3 (US\_REG3) (continued)**

## **10.4 Data registers**



#### **Table 65. DSP live event 1 (DSP\_EV1)**



<b>Row</b>	<b>Bit</b>	Internal signal	<b>Description</b>	<b>Default</b>
21	19		Primary voltage zero-crossing	0
	20		Primary voltage sigma-delta bitstream stuck	0
	21		Primary voltage period error (out of range)	0
	22			0
	23	V1 events	Primary voltage swell event history	0
	24			0
	25			0
	26		Primary voltage sag event history	0
	27			0
	28			0
	29			0
	30		Reserved	$\Omega$
	31		Reserved	$\Omega$

**Table 65. DSP live event 1 (DSP\_EV1) (continued)**

#### **Table 66. DSP live event 2 (DSP\_EV2)**





Row	<b>Bit</b>	Internal signal	<b>Description</b>	<b>Default</b>
	12		Secondary current zero-crossing	0
	13	C <sub>2</sub> events V <sub>2</sub> events	Secondary current sigma-delta bitstream stuck	$\Omega$
	14		Secondary current AH accumulation	0
	15			$\Omega$
	16		Secondary current swell event history	0
	17			$\Omega$
	18			$\Omega$
	19		Secondary voltage zero-crossing	0
	20		Secondary voltage sigma-delta bitstream stuck	0
22	21		Secondary voltage period error (out of range)	$\Omega$
	22		Secondary voltage swell event history	$\Omega$
	23			$\Omega$
	24			$\Omega$
	25			$\mathbf 0$
	26			$\Omega$
	27		Secondary voltage sag event history	0
	28			0
	29			0
	30		Reserved	$\Omega$
	31		Reserved	0

**Table 66. DSP live event 2 (DSP\_EV2) (continued)**



## **11 Package mechanical data**

In order to meet environmental requirements, ST offers these devices in different grades of ECOPACK® packages, depending on their level of environmental compliance. ECOPACK® specifications, grade definitions and product status are available at:www.st.com. ECOPACK® is an ST trademark.



## **11.1 QFN24L 4x4x1 mm 0.5 pitch**



**Figure 49. QFN24L 4x4x1 mm 0.5 pitch drawings**









#### **Figure 50. QFN24L 4x4x1 recommended footprint**



## **11.2 QFN32L 5x5x1 mm 0.5 pitch**



**Figure 51. QFN32L 5x5x1 mm 0.5 pitch drawings**

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<b>P.A.</b>			
Symbol	mm		
	Min.	Typ.	Max.
A	0.80	0.90	1.00
A1	0.00	0.02	0.05
A <sub>3</sub>		0.20	
b	0.18	0.25	0.30
D	4.85	5.00	5.15
D <sub>2</sub>	3.40	3.45	3.50
E	4.85	5.00	5.15
E <sub>2</sub>	3.40	3.45	3.50
$\mathbf e$	0.45	0.50	0.55
L	0.30	0.40	0.50
Ddd			0.08

**Table 68. QFN32L 5x5x1 mm 0.5 pitch mechanical data**



# **12 Revision history**

#### **Table 69. Revision history**





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